

Instructor: Minchen Li

$$\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \nabla \vec{u} + \frac{1}{\rho} \nabla p = \vec{g} + \nu \nabla \cdot \nabla \vec{u},$$
$$\nabla \cdot \vec{u} = 0.$$

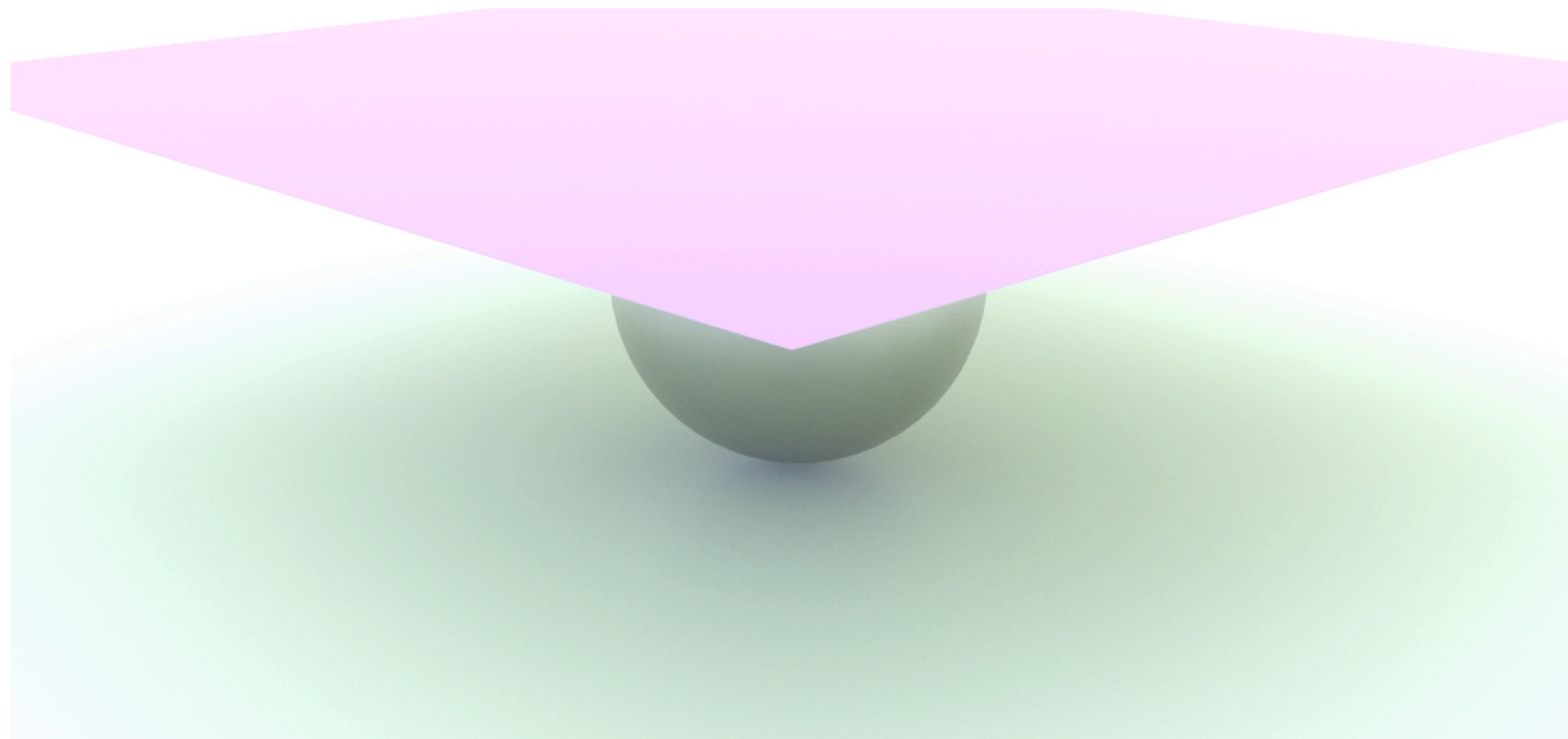


Lec 15: Fluid Simulation Fundamentals, SPH

15-769: Physically-based Animation of Solids and Fluids (F23)

Recap: Codimensional Solids – Thin Shells

Simulating Using Surface Meshes

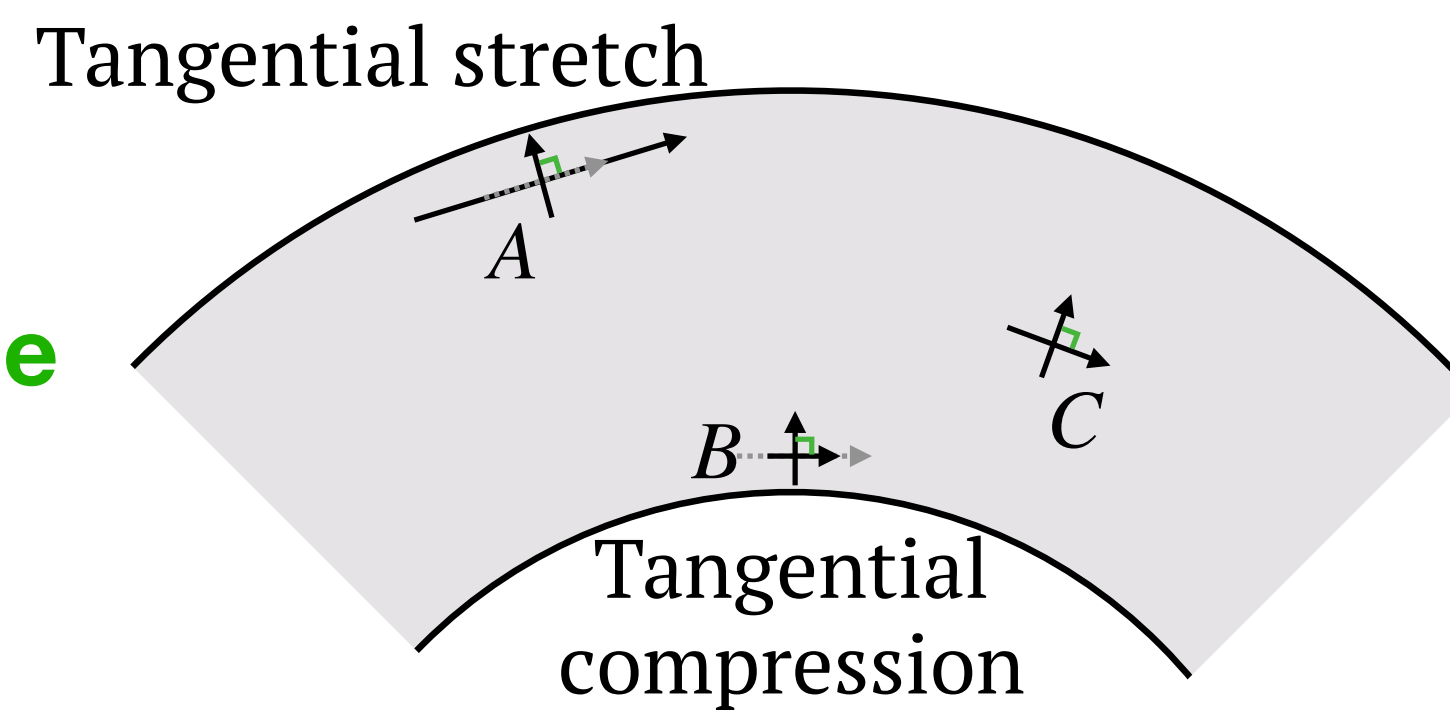


Avoid ill-conditioning:

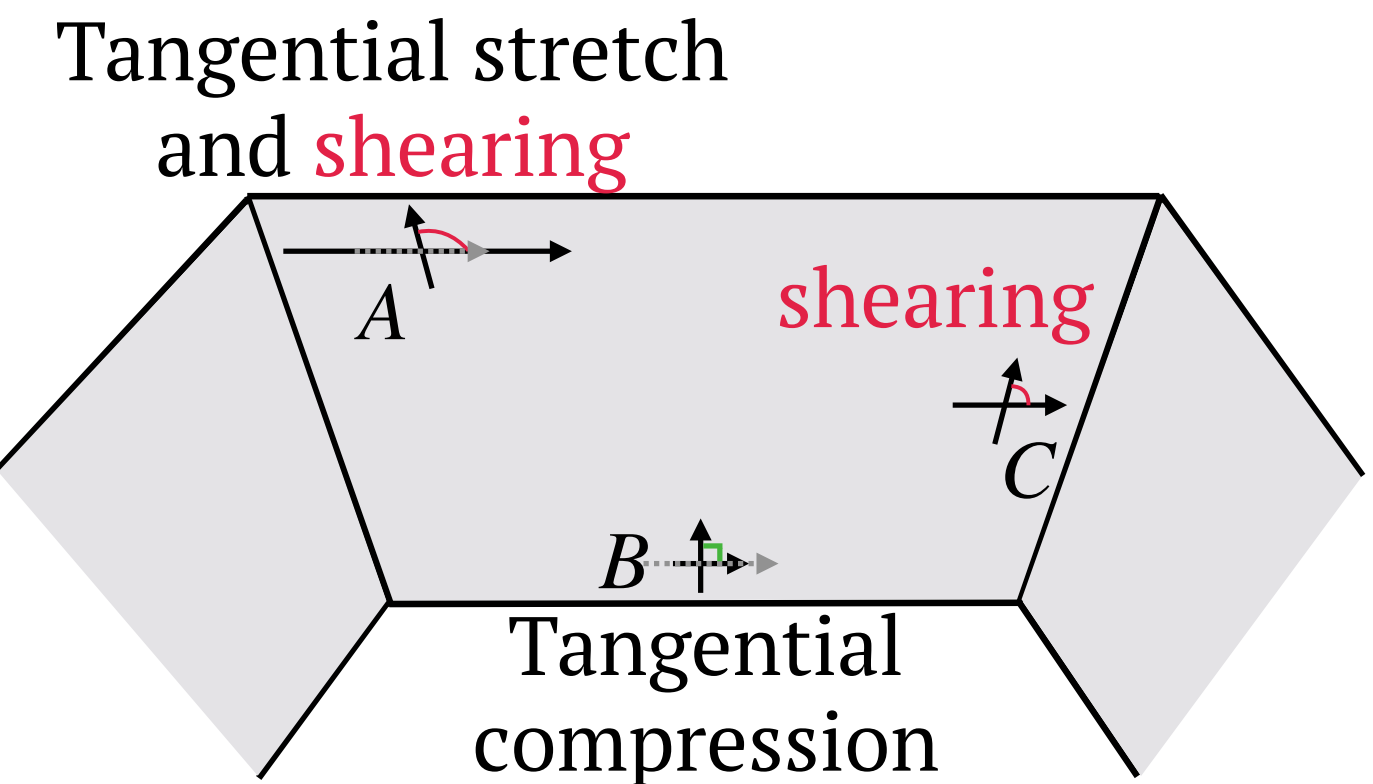


Avoid shear locking issue
(linear shape functions):

Higher-order shape
functions are expensive



(a) Ideal Setting

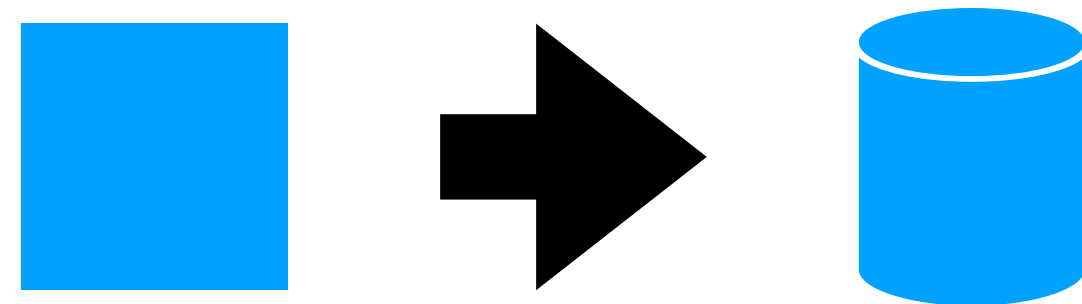


(b) Coarse Tessellation with Linear Basis

Recap: Codimensional Solids – Thin Shells

Bending Energy

With only tangent space elasticity, no force under isometric deformation:



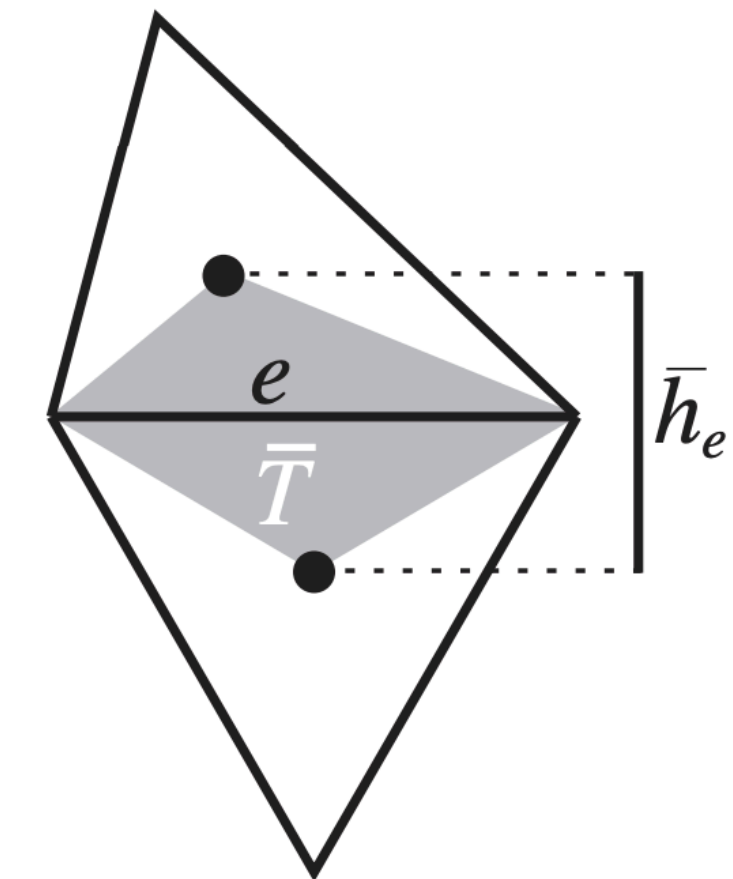
Model the strain energy for bending directly as a penalty of mean curvature changes

$$\int_{\bar{\Omega}} (H \circ \varphi - \bar{H})^2 d\bar{A}$$

After discretization:

$$\Psi_{\text{bend}}(x) = \sum_i k \frac{3 \|\bar{e}_i\|^2}{\bar{A}_i} (\theta_i - \bar{\theta}_i)^2$$

$$k = \frac{E\xi^3}{24(1-\nu^2)}$$



Garg et al. [2007]:
For isometric deformation,
A bending energy can be formulated as
a **cubic** polynomial of x

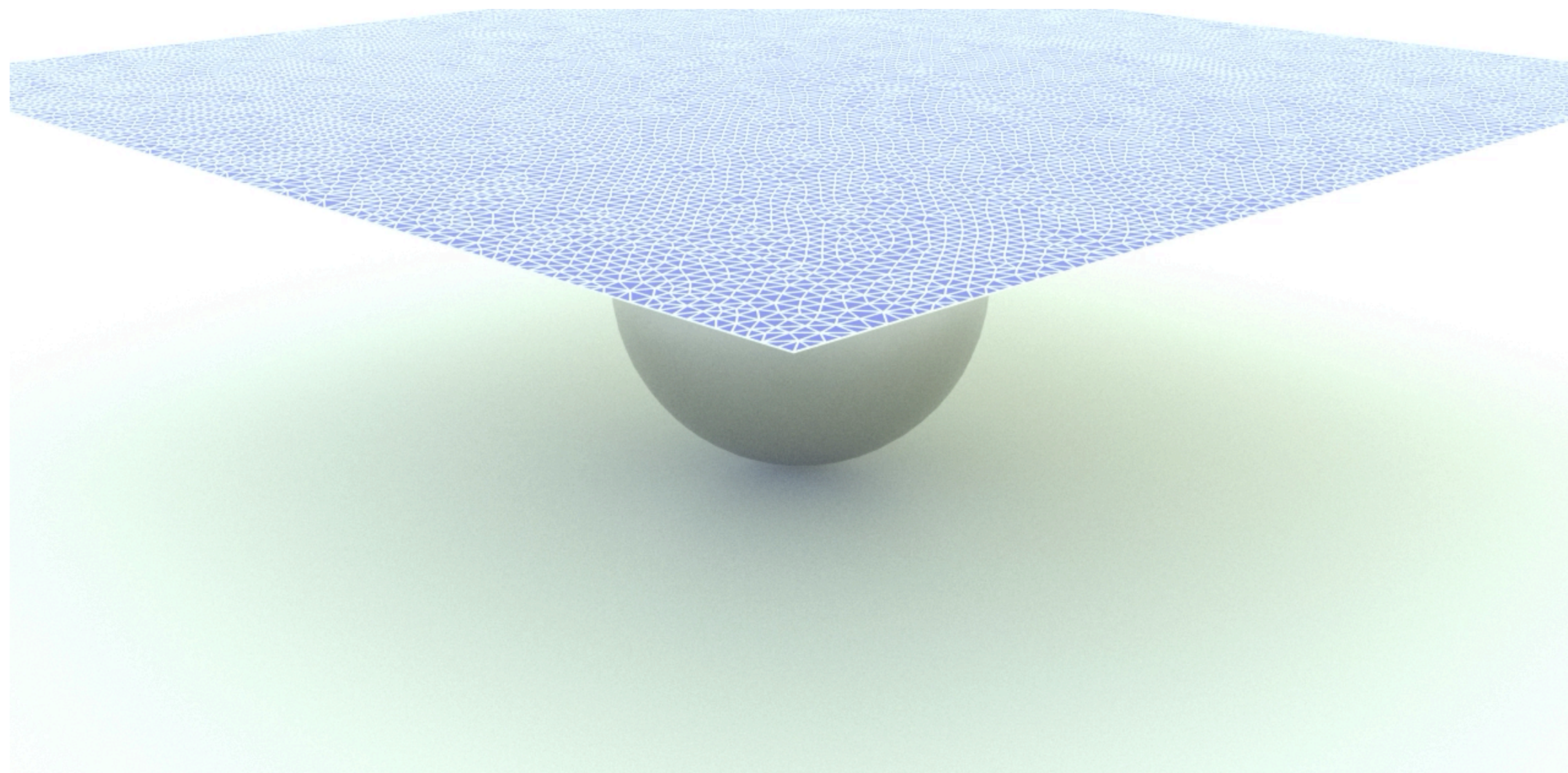
Bergou et al. [2006]:
For isometric deformation of plates (flat rest shapes),
A bending energy can be formulated as
a **quadratic** polynomial of x

Recap: Codimensional Solids – Thin Shells

Membrane Locking

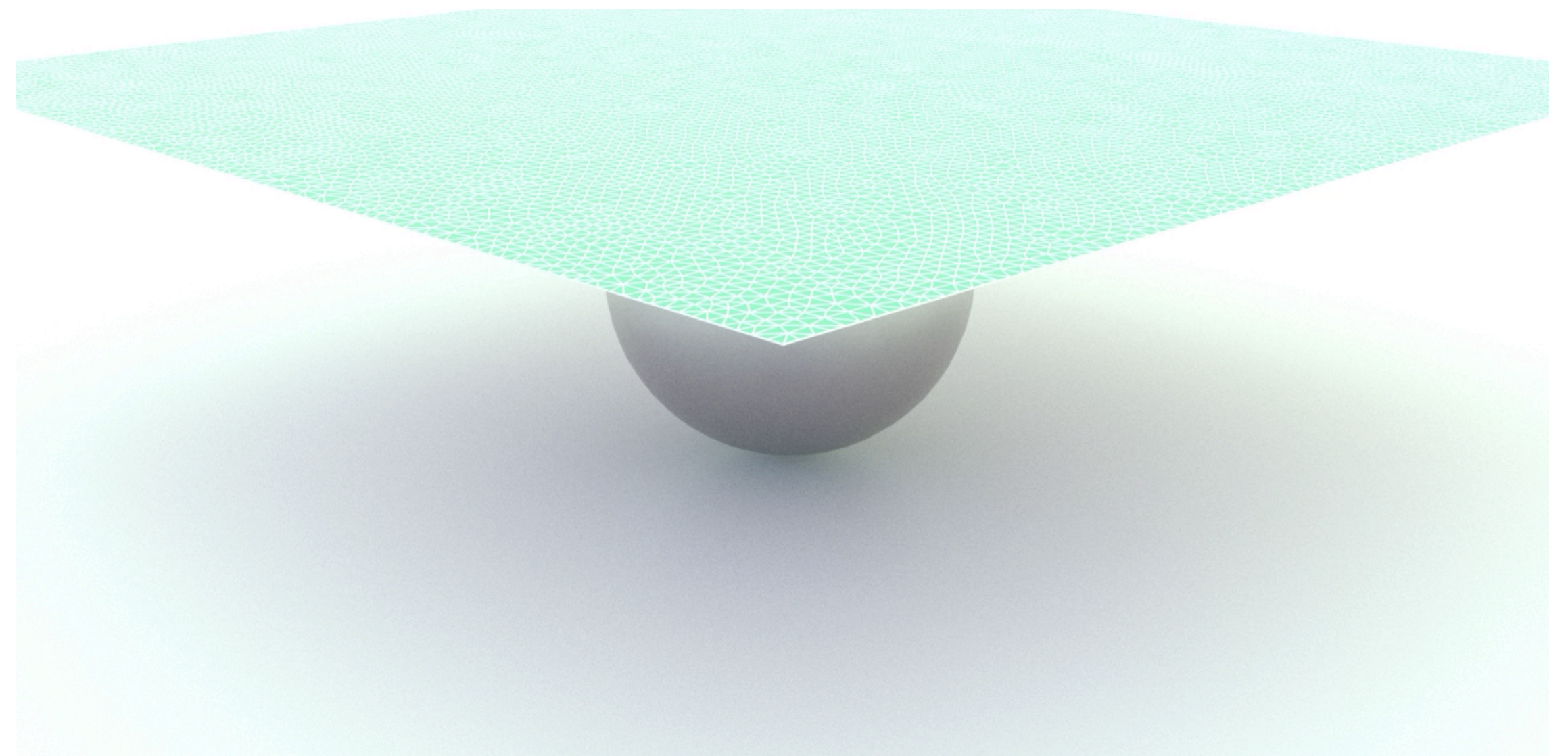
Cloth are nearly unstretchable – stiff stretch resistance, $E = \sim 10^7$ Pa

With low-res triangulation, there can be geometric lockings:



Stiff membrane creates extra bending penalty
(real material parameter)

Solution:
Softer material parameters + **Strain limiting**



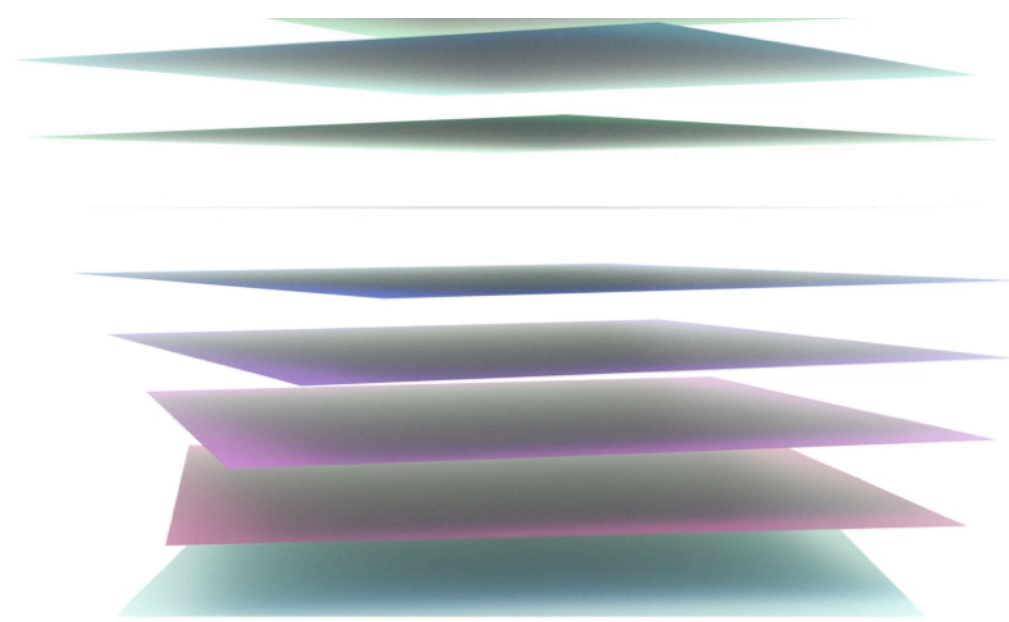
0.01x membrane stiffness + 10% strain limit

Recap: Codimensional Solids – Thin Shells

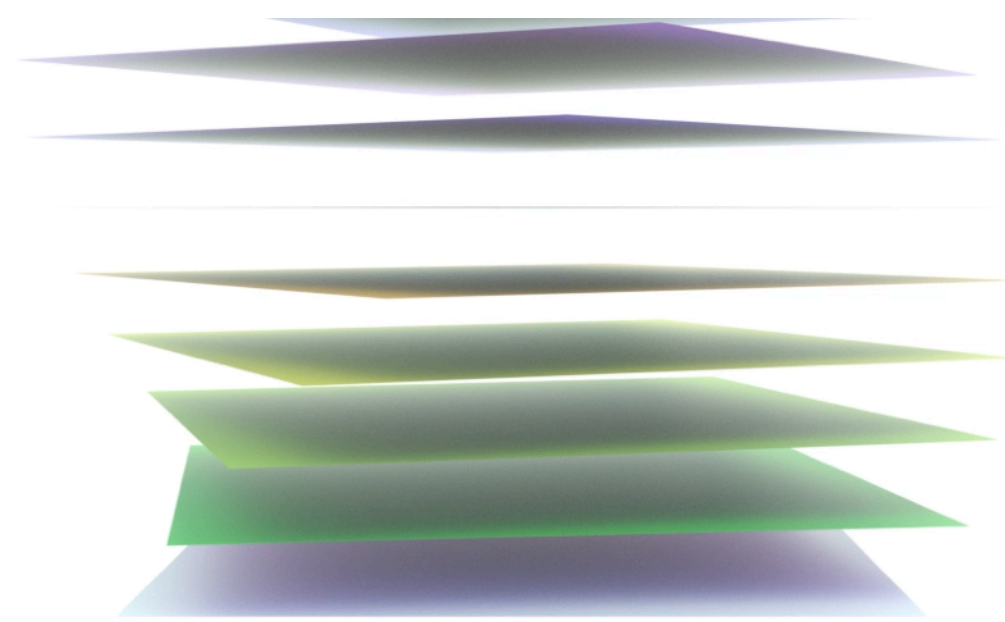
Thickness Modeling

Using IPC:

Elastic Thickness

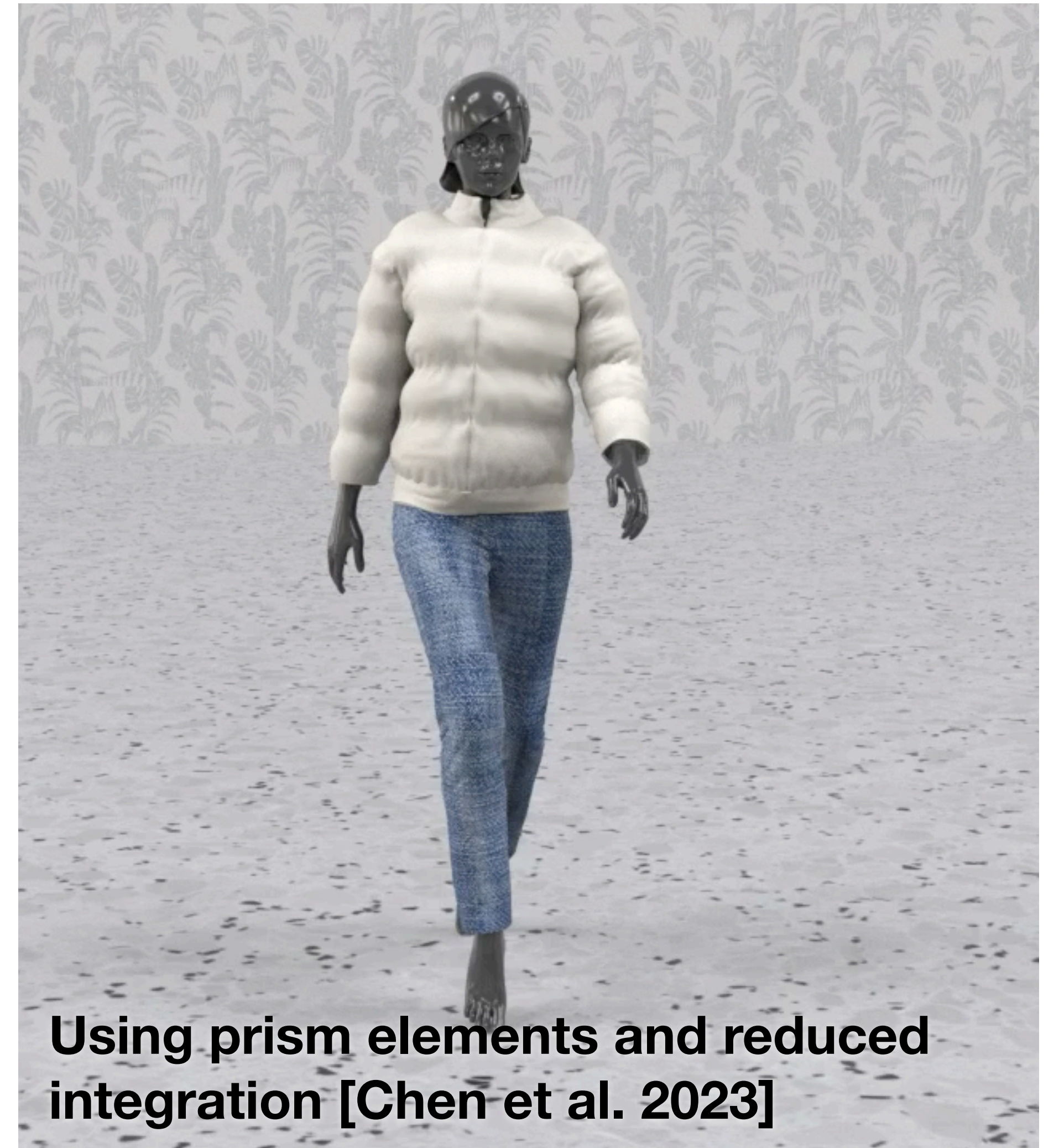


$\hat{d} = 1mm$



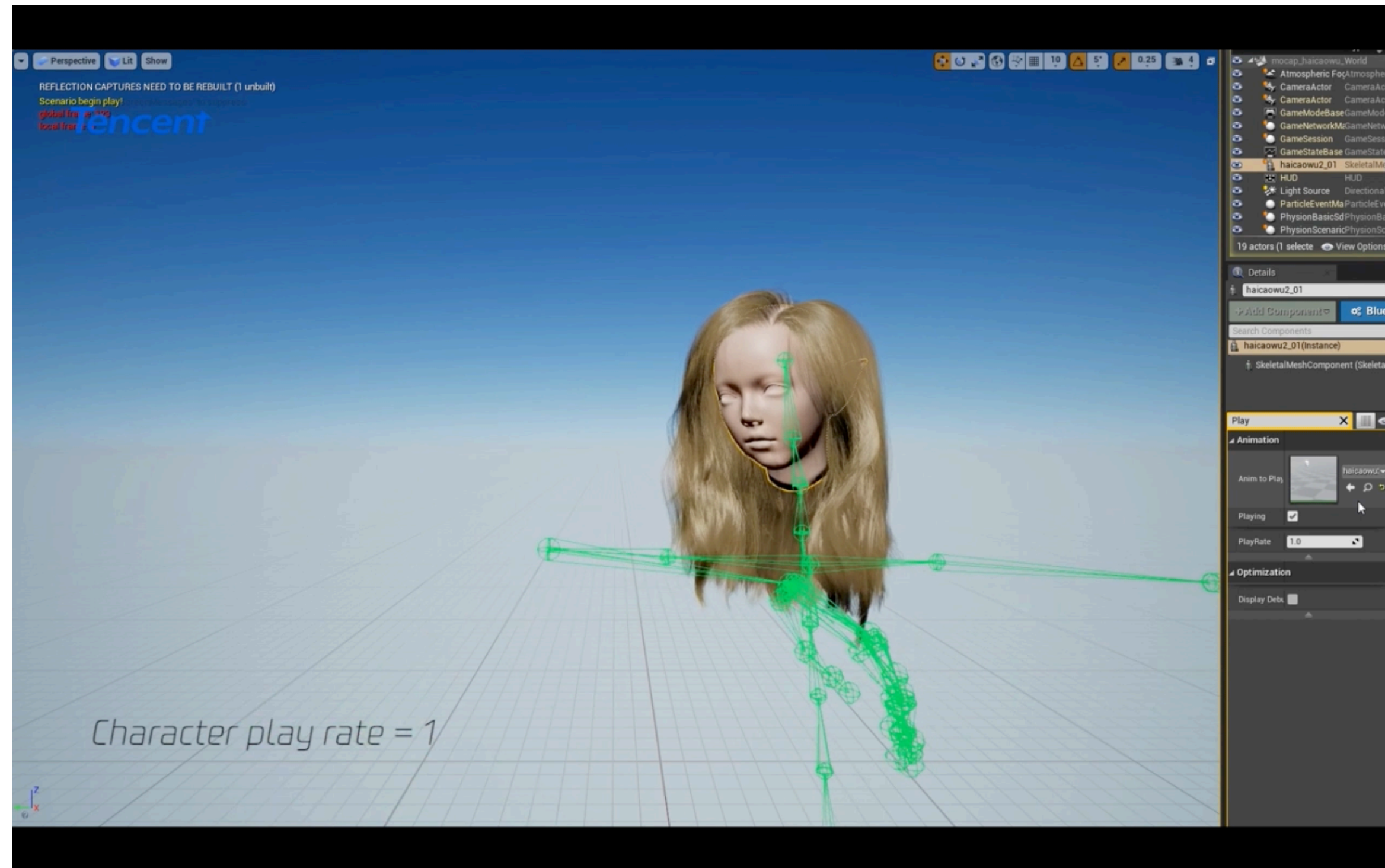
$\hat{d} = 10mm$

Inelastic Thickness (Contact Gap)

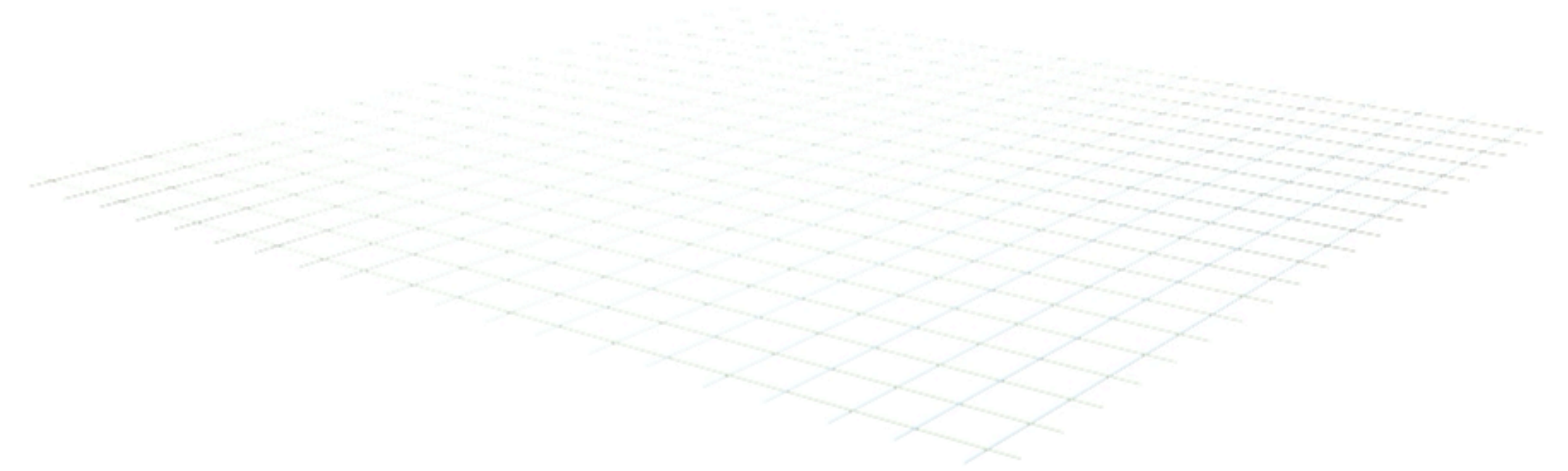


Using prism elements and reduced integration [Chen et al. 2023]

Recap: Codimensional Solids – Rods and Particles



Hair simulation [Huang et al. 2023] based on Discrete Elastic Rod and MPM



Coupling codimension-0,1,2,3 solids using IPC

Today: Fluid Simulation

Fluid as a Special Kind of Solid

- Fluid: as a special kind of solid whose strain energy only penalizes volume change
 - i.e. no resistance to volume-preserving shearing, nor rotation
 - Dissipative effects can be modeled via viscosity

$$x^{n+1} = \arg \min_x \frac{1}{2} \|x - \tilde{x}^n\|^2 + h^2 \sum P(x) \quad \text{e.g. } P_{fluid}(x) = \sum_e V_e^0 \frac{\kappa}{2} (\det(\mathbf{F}_e(x)) - 1)^2$$

Frequent and large topology changes -> **mesh quality gets really bad!**

Frequent remeshing is not practical!

Simulating Fluids in Eulerian View using Particles

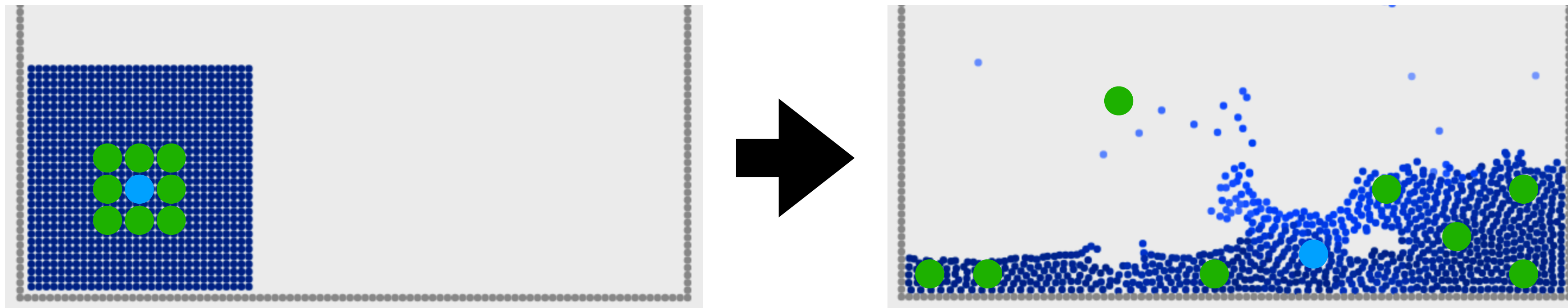
Use particles to track/represent fluid regions

(The particles are macroscopic markers, not molecules!)

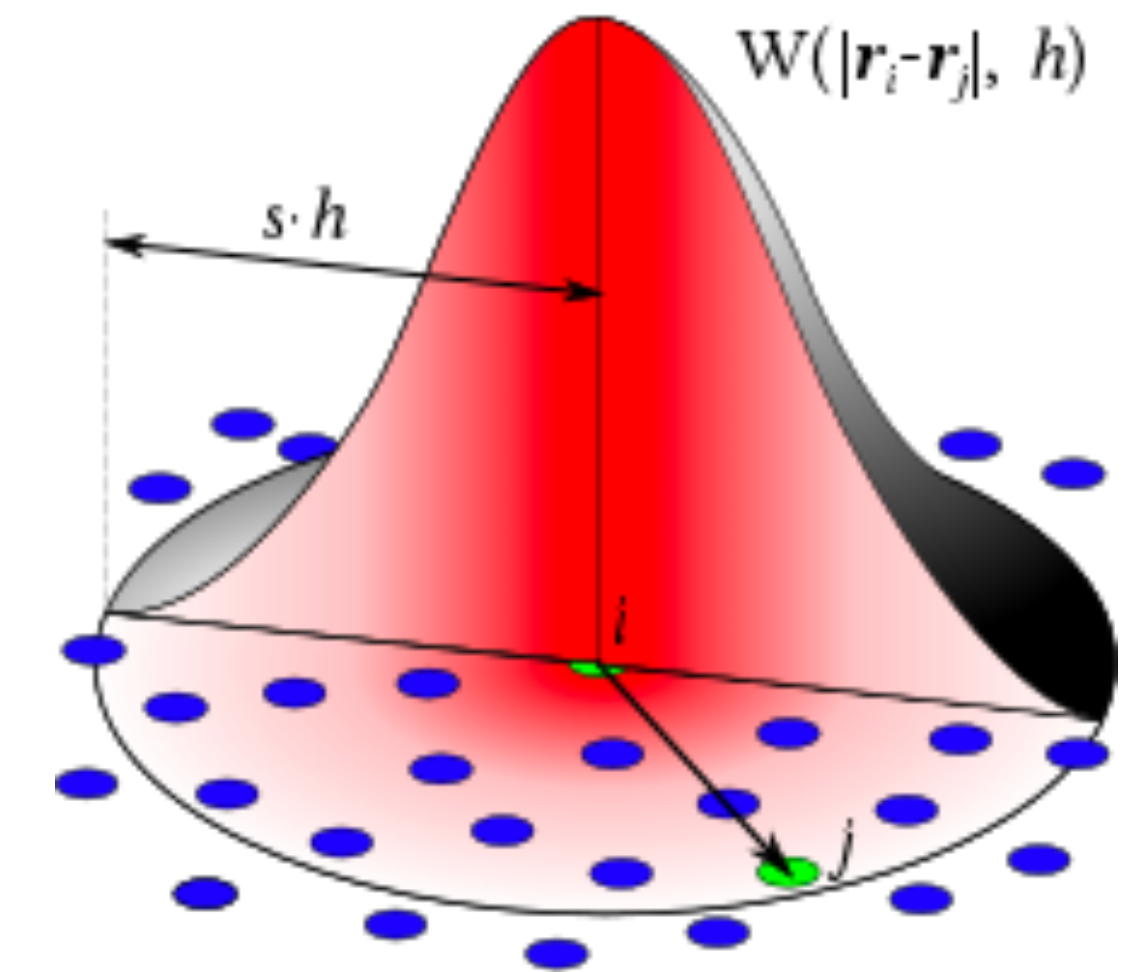
Use shape functions directly defined in space (not on meshes)

Topology change gets easy!

Material-space shape functions can barely work:

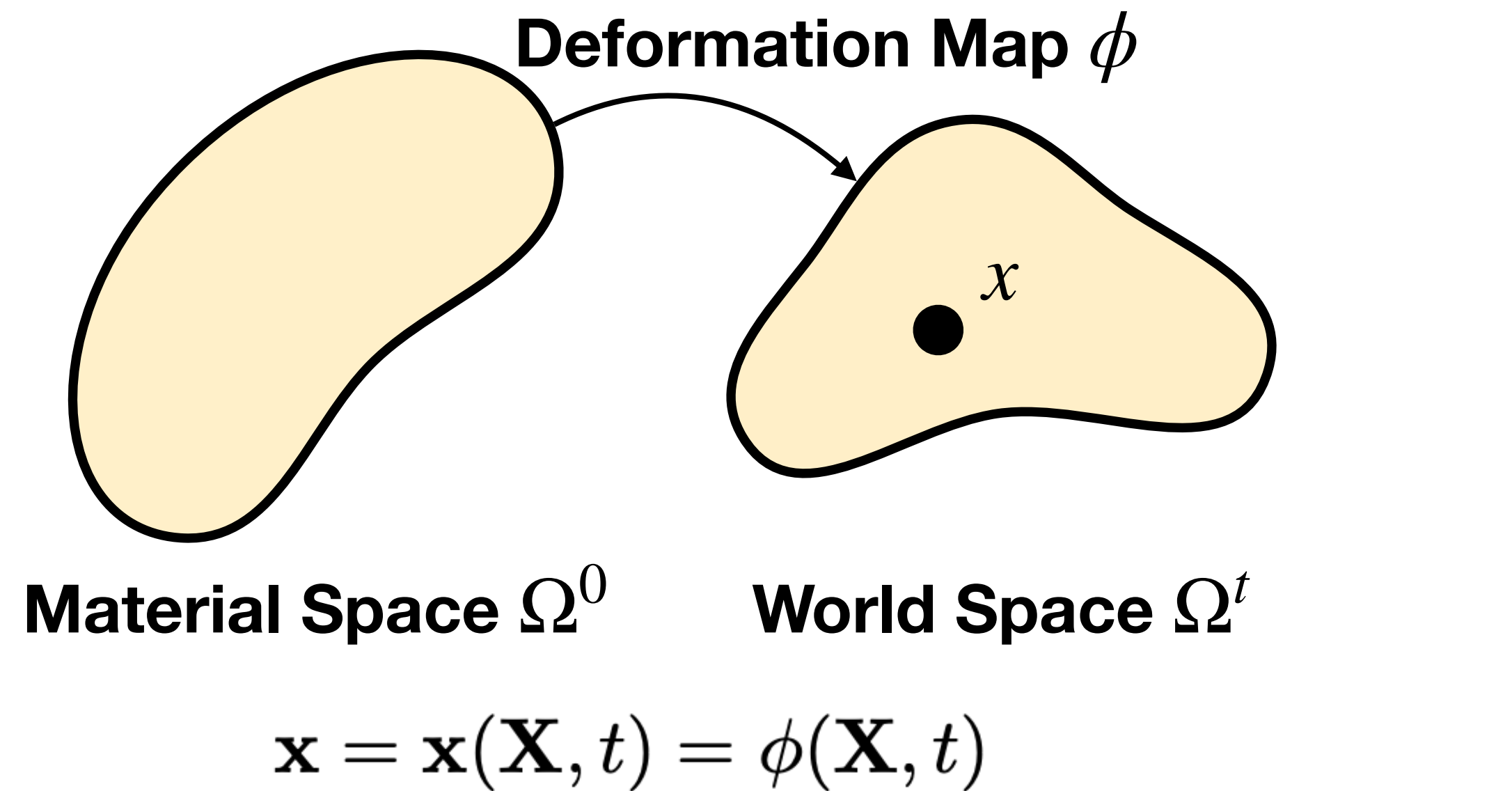


Use world-space shape functions! (Eulerian view)*



*Using world-space shape functions in Eulerian simulation, the time integration is subject to CFL conditions.

Lagrangian v.s Eulerian View



$$\mathbf{X} = \phi^{-1}(\mathbf{x}, t)$$

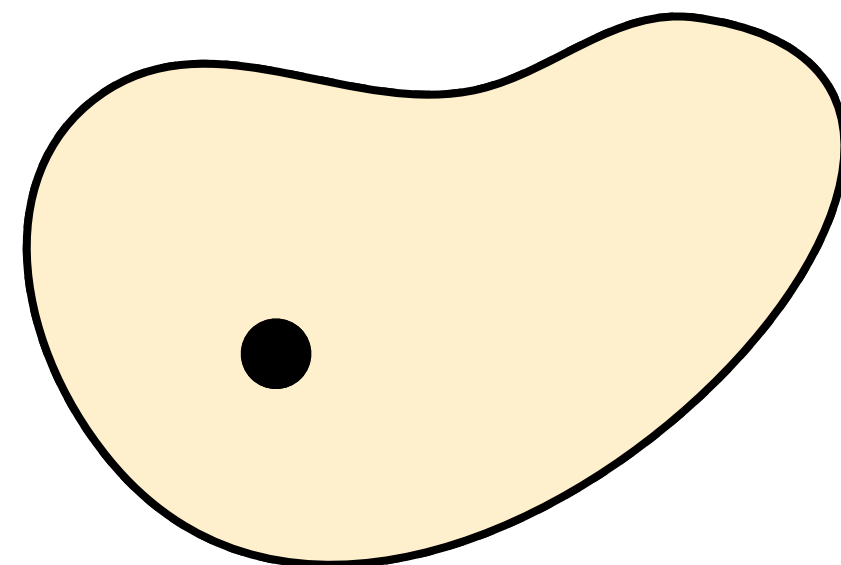
$$\mathbf{Q}(\mathbf{X}, t) = \mathbf{Q}(\phi^{-1}(\mathbf{x}, t), t) \equiv \mathbf{q}(\mathbf{x}, t)$$

– Push forward

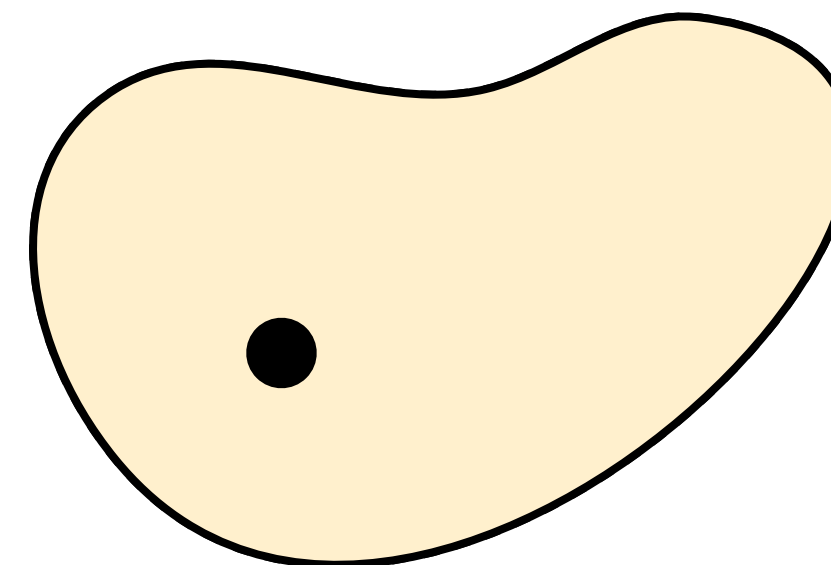
Pull back:

$$\mathbf{q}(\mathbf{x}, t) = \mathbf{q}(\phi(\mathbf{X}, t), t) \equiv \mathbf{Q}(\mathbf{X}, t)$$

Lagrangian view:
Quantity measured
at **a point on the solid**



Eulerian view:
Quantity measured
at **a point in space**



Lagrangian v.s Eulerian View

The Material Derivative of Eulerian Quantities

$$\mathbf{x} = \mathbf{x}(\mathbf{X}, t) = \phi(\mathbf{X}, t) \quad \mathbf{X} = \phi^{-1}(\mathbf{x}, t)$$

Push forward: $\mathbf{Q}(\mathbf{X}, t) = \mathbf{Q}(\phi^{-1}(\mathbf{x}, t), t) \equiv \mathbf{q}(\mathbf{x}, t)$ **Pull back:** $\mathbf{q}(\mathbf{x}, t) = \mathbf{q}(\phi(\mathbf{X}, t), t) \equiv \mathbf{Q}(\mathbf{X}, t)$

$$\mathbf{V}(\mathbf{X}, t) = \frac{\partial \phi}{\partial t}(\mathbf{X}, t)$$

$$\mathbf{A}(\mathbf{X}, t) = \frac{\partial^2 \phi}{\partial t^2}(\mathbf{X}, t) = \frac{\partial \mathbf{V}}{\partial t}(\mathbf{X}, t).$$

$$\mathbf{v}(\mathbf{x}, t) = \mathbf{V}(\phi^{-1}(\mathbf{x}, t), t),$$

$$\mathbf{a}(\mathbf{x}, t) = \mathbf{A}(\phi^{-1}(\mathbf{x}, t), t).$$

$$\mathbf{V}(\mathbf{X}, t) = \mathbf{v}(\phi(\mathbf{X}, t), t),$$

$$\mathbf{A}(\mathbf{X}, t) = \mathbf{a}(\phi(\mathbf{X}, t), t).$$

$$\mathbf{A}(\mathbf{X}, t) = \frac{\partial}{\partial t} \mathbf{V}(\mathbf{X}, t) = \frac{\partial \mathbf{v}}{\partial t}(\phi(\mathbf{X}, t), t) + \frac{\partial \mathbf{v}}{\partial \mathbf{x}}(\phi(\mathbf{X}, t), t) \frac{\partial \phi}{\partial t}(\mathbf{X}, t).$$

$$A_i(\mathbf{X}, t) = \frac{\partial}{\partial t} V_i(\mathbf{X}, t) = \frac{\partial v_i}{\partial t}(\phi(\mathbf{X}, t), t) + \frac{\partial v_i}{\partial x_j}(\phi(\mathbf{X}, t), t) \frac{\partial \phi_j}{\partial t}(\mathbf{X}, t).$$

$$a_i(\mathbf{x}, t) = A_i(\phi^{-1}(\mathbf{x}, t), t) = \frac{\partial v_i}{\partial t}(\mathbf{x}, t) + \frac{\partial v_i}{\partial x_j}(\mathbf{x}, t) v_j(\mathbf{x}, t)$$

$$\boxed{a_i(\mathbf{x}, t) \neq \frac{\partial v_i}{\partial t}(\mathbf{x}, t).}$$

$$\boxed{\mathbf{a}(\mathbf{x}, t) = \frac{D\mathbf{v}(\mathbf{x}, t)}{Dt}}$$

(Material Derivative)

Conservation of Momentum

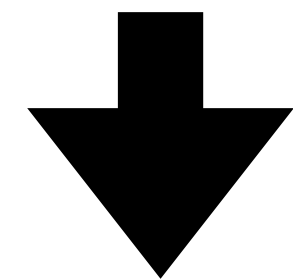
Lagrangian View: $R(\mathbf{X}, 0) \frac{\partial \mathbf{V}}{\partial t}(\mathbf{X}, t) = \nabla^{\mathbf{X}} \cdot \mathbf{P}(\mathbf{X}, t) + R(\mathbf{X}, 0) \mathbf{g}$

Newton's 2nd Law on B_ϵ^0 :

$$\int_{B_\epsilon^0} R(\mathbf{X}, 0) \frac{\partial \mathbf{V}}{\partial t}(\mathbf{X}, t) d\mathbf{X} = \int_{\partial B_\epsilon^0} \mathbf{P}(\mathbf{X}, t) \mathbf{N}(\mathbf{X}) ds(\mathbf{X}) + \int_{B_\epsilon^0} R(\mathbf{X}, 0) \mathbf{A}^{\text{ext}}(\mathbf{X}, t) d\mathbf{X}, \quad \forall B_\epsilon^0 \subset \Omega^0 \text{ and } t \geq 0.$$

Applying Divergence Theorem:

$$\int_{B_\epsilon^0} R(\mathbf{X}, 0) \frac{\partial \mathbf{V}}{\partial t}(\mathbf{X}, t) d\mathbf{X} = \int_{B_\epsilon^0} \nabla^{\mathbf{X}} \cdot \mathbf{P}(\mathbf{X}, t) d\mathbf{X} + \int_{B_\epsilon^0} R(\mathbf{X}, 0) \mathbf{A}^{\text{ext}}(\mathbf{X}, t) d\mathbf{X}, \quad \forall B_\epsilon^0 \subset \Omega^0 \text{ and } t \geq 0.$$



Push forward and extract the integrand

Eulerian View: $\rho(\mathbf{x}, t) \frac{D\mathbf{v}}{Dt}(\mathbf{x}, t) = \nabla^{\mathbf{x}} \cdot \boldsymbol{\sigma}(\mathbf{x}, t) + \rho(\mathbf{x}, t) \mathbf{g}$

Cauchy stress: $\boldsymbol{\sigma} = \frac{1}{J} \mathbf{P} \mathbf{F}^T$ $Q_{i,j} = \frac{\partial Q_i}{\partial X_j} = \frac{\partial q_i}{\partial x_k} \frac{\partial x_k}{\partial X_j} = q_{i,k} F_{kj}$ $d\mathbf{X} = \frac{1}{J} d\mathbf{x}$

Inviscid Navier-Stoke's Equation

How is Cauchy stress modeled?

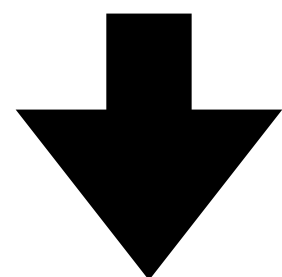
Consider a fluid constitutive model, e.g. $\Psi_{fluid}(\mathbf{F}) = \frac{\kappa}{2}(\det(\mathbf{F}) - 1)^2$

$$\mathbf{P} = \frac{\partial \Psi}{\partial \mathbf{F}} = \frac{\partial \Psi}{\partial J} \frac{\partial J}{\partial \mathbf{F}} = \kappa(J - 1)J\mathbf{F}^{-T}$$

$$\boldsymbol{\sigma} = \frac{1}{J}\mathbf{P}\mathbf{F}^T = \kappa(J - 1)\mathbf{I} = -p\mathbf{I}$$

$$p = -\frac{\partial \Psi}{\partial J} \text{ is called Pressure}$$

Momentum Conservation (Eulerian View): $\rho(\mathbf{x}, t)\frac{D\mathbf{v}}{Dt}(\mathbf{x}, t) = \nabla^{\mathbf{x}} \cdot \boldsymbol{\sigma}(\mathbf{x}, t) + \rho(\mathbf{x}, t)\mathbf{g}$



$$\rho\frac{D\mathbf{v}}{Dt} = -\nabla_{\mathbf{x}}p + \rho\mathbf{g}$$

– Euler Equation

– Navier Stoke's Equation (Inviscid)

$$\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \nabla \vec{u} + \frac{1}{\rho} \nabla p = \vec{g}$$

Incompressibility

Consider a fluid constitutive model, e.g. $\Psi_{fluid}(\mathbf{F}) = \frac{\kappa}{2}(\det(\mathbf{F}) - 1)^2$

κ is called bulk modulus, similar to Young's modulus for solids

How large should κ be?

| | |
|-------|---------|
| Water | 2.2 GPa |
|-------|---------|

Very stiff!

(en.wikipedia.org/wiki/Bulk_modulus)

What if we model volume-preserving fluids using equality constraints?

Applying divergence theorem:

$$\frac{d}{dt}V(B_e^t) = \int_{\partial B_e^t} \mathbf{v} \cdot \mathbf{n} d\mathbf{x} = 0 \quad \forall B_e^t \in \Omega^t \quad \longleftrightarrow \quad \int_{B_e^t} \nabla \cdot \mathbf{v} d\mathbf{x} = 0 \quad \forall B_e^t \in \Omega^t \quad \longleftrightarrow \quad \nabla \cdot \mathbf{v} = 0$$

Incompressible Navier-Stoke's Equation (Inviscid):

$$\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \nabla \vec{u} + \frac{1}{\rho} \nabla p = \vec{g}$$

$$\nabla \cdot \vec{u} = 0.$$

Lagrange multiplier term

Solving the KKT is still hard, But magic tricks can be applied!

Viscosity

Can be viewed as fluid friction – penalizing stretching and shearing motion

Strain rate tensor: $\mathbf{D} = \frac{1}{2}(\nabla \mathbf{v} + \nabla \mathbf{v}^T)$

Newtonian fluids: $\sigma_{viscosity} = 2\mu\mathbf{D} + \lambda\text{tr}(\mathbf{D})\mathbf{I}$

$$\rho(\mathbf{x}, t) \frac{D\mathbf{v}}{Dt}(\mathbf{x}, t) = \nabla^{\mathbf{x}} \cdot \sigma(\mathbf{x}, t) + \rho(\mathbf{x}, t)\mathbf{g}$$

Newtonian fluids: $\sigma = -p\mathbf{I} + \mu(\nabla \mathbf{v} + \nabla \mathbf{v}^T) + \lambda\text{tr}(\mathbf{D})\mathbf{I}$

tr(D) = ∇ · v = 0 for incompressible fluids

$$\nabla \cdot (\mu(\nabla \mathbf{v} + \nabla \mathbf{v}^T)) = \mu(\nabla \cdot \nabla \mathbf{v} + \nabla \cdot (\nabla \mathbf{v})^T)$$

$$\nabla \cdot \begin{bmatrix} \frac{\partial \mathbf{v}}{\partial x_1}^T \\ \frac{\partial \mathbf{v}}{\partial x_2}^T \\ \frac{\partial \mathbf{v}}{\partial x_3}^T \end{bmatrix} = \begin{bmatrix} \frac{\partial}{\partial x_1} \sum_i \frac{\partial v_i}{\partial x_i} \\ \frac{\partial}{\partial x_2} \sum_i \frac{\partial v_i}{\partial x_i} \\ \frac{\partial}{\partial x_3} \sum_i \frac{\partial v_i}{\partial x_i} \end{bmatrix} = \nabla(\nabla \cdot \mathbf{v}) = 0$$

for incompressible fluids

Incompressible Navier-Stoke's Equation

$$\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \nabla \vec{u} + \frac{1}{\rho} \nabla p = \vec{g} + \nu \nabla \cdot \nabla \vec{u},$$

$$\nabla \cdot \vec{u} = 0.$$

Time Splitting

Consider a generic ODE:

$$\frac{dq}{dt} = f(q) + g(q).$$

Explicit time integration with splitting:

$$\tilde{q} = q^n + \Delta t f(q^n),$$

$$q^{n+1} = \tilde{q} + \Delta t g(\tilde{q}).$$

$$q^{n+1} = (q^n + \Delta t f(q^n)) + \Delta t g(q^n + \Delta t f(q^n))$$

$$= q^n + \Delta t f(q^n) + \Delta t (g(q^n) + O(\Delta t))$$

$$= q^n + \Delta t (f(q^n) + g(q^n)) + O(\Delta t^2)$$

$$= \boxed{q^n + \frac{dq}{dt} \Delta t} + O(\Delta t^2).$$

Explicit Euler

Incompressible Navier-Stoke's Equation

$$\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \nabla \vec{u} + \frac{1}{\rho} \nabla p = \vec{g} + \nu \nabla \cdot \nabla \vec{u},$$
$$\nabla \cdot \vec{u} = 0.$$

For each time step n :

$$u^a \leftarrow \text{Solve } \frac{\partial u}{\partial t} + u \cdot \nabla u = 0 \text{ (advection)}$$

$$u^b \leftarrow \text{Solve } \frac{\partial u}{\partial t} = g \text{ (apply external force)}$$

$$u^c \leftarrow \text{Solve } \frac{\partial u}{\partial t} = \nu \nabla \cdot \nabla u \text{ (diffusion)}$$

$$u^{n+1} \leftarrow \text{Solve } \nabla \cdot u = 0 \text{ (pressure projection)}$$

With constraint view, this step is stable!

The Smoothed Particle Hydrodynamics (SPH) Method

A Brief Introduction

Given a field A and a smoothing kernel function W , e.g. Gaussian

A smoother version of A as an approximation of it is

$$A(\mathbf{x}) \approx (A * W)(\mathbf{x}) = \int A(\mathbf{x}') W(\mathbf{x} - \mathbf{x}', h) dv'$$

Favored properties of W :

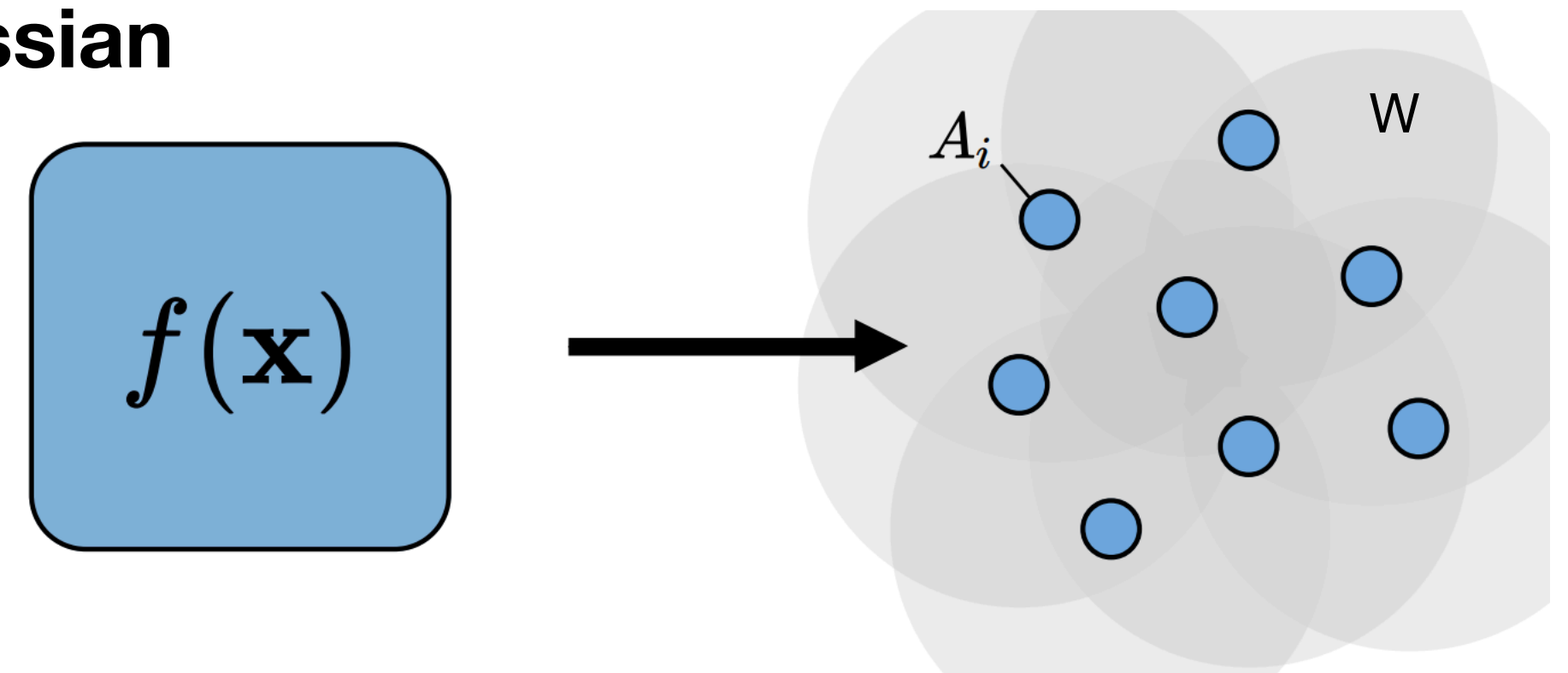
$$\int_{\mathbb{R}^d} W(\mathbf{r}', h) dv' = 1 \quad (\text{normalization condition})$$

$$\lim_{h' \rightarrow 0} W(\mathbf{r}, h') = \delta(\mathbf{r}) \quad (\text{Dirac-}\delta \text{ condition})$$

$$W(\mathbf{r}, h) \geq 0 \quad (\text{positivity condition})$$

$$W(\mathbf{r}, h) = W(-\mathbf{r}, h) \quad (\text{symmetry condition})$$

$$W(\mathbf{r}, h) = 0 \text{ for } \|\mathbf{r}\| \geq \tilde{h}, \quad (\text{compact support condition})$$



Discretization using particles:

$$(A * W)(\mathbf{x}_i) = \int \frac{A(\mathbf{x}')}{\rho(\mathbf{x}')} W(\mathbf{x} - \mathbf{x}', h) \underbrace{\rho(\mathbf{x}')}_{dm'} dv' \\ \approx \sum_{j \in \mathcal{F}} A_j \frac{m_j}{\rho_j} W(\mathbf{x}_i - \mathbf{x}_j, h) =: \langle A(\mathbf{x}_i) \rangle$$

The kernel needs to involve a large number of neighbors for accurate estimation!

A Brief Introduction to SPH

To solve the incompressible Navier-Stoke's Equation

$$\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \nabla \vec{u} + \frac{1}{\rho} \nabla p = \vec{g} + \nu \nabla \cdot \nabla \vec{u},$$
$$\nabla \cdot \vec{u} = 0.$$

Just need to approximate the differential operators,
And relate velocity to pressure via constitutive models

Direct discretization are not accurate
and can lead to instability:

$$\nabla \mathbf{A}_i \approx \sum_j \frac{m_j}{\rho_j} \mathbf{A}_j \otimes \nabla W_{ij}$$
$$\nabla \cdot \mathbf{A}_i \approx \sum_j \frac{m_j}{\rho_j} \mathbf{A}_j \cdot \nabla W_{ij}$$

Difference and symmetric
formula are often used:

$$\nabla A_i \approx \langle \nabla A_i \rangle - A_i \langle \nabla 1 \rangle$$
$$= \sum_j \frac{m_j}{\rho_j} (A_j - A_i) \nabla_i W_{ij}.$$

$$\nabla A_i \approx \rho_i \left(\frac{A_i}{\rho_i^2} \langle \nabla \rho \rangle + \langle \nabla \left(\frac{A_i}{\rho_i} \right) \rangle \right)$$
$$= \rho_i \sum_j m_j \left(\frac{A_i}{\rho_i^2} + \frac{A_j}{\rho_j^2} \right) \nabla_i W_{ij}.$$

A Brief Introduction to SPH

To solve the incompressible Navier-Stoke's Equation

$$\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \nabla \vec{u} + \frac{1}{\rho} \nabla p = \vec{g} + \nu \nabla \cdot \nabla \vec{u},$$
$$\nabla \cdot \vec{u} = 0.$$

Just need to approximate the differential operators,
And relate velocity to pressure via constitutive models

Relate velocity to pressure via state equation:

$$p = - \frac{\partial \Psi}{\partial J} \quad \text{e.g. } p = - \kappa(J - 1) \text{ for } \Psi = \frac{\kappa}{2}(J - 1)^2$$

– Weakly-Compressible SPH, or WCSPH

Handling pressure term by
solving $\nabla \cdot u = 0$:

- Implicit Incompressible SPH (IISPH)
- Divergence-Free SPH (DFSPH)

A Brief Introduction to SPH

To solve the incompressible Navier-Stoke's Equation

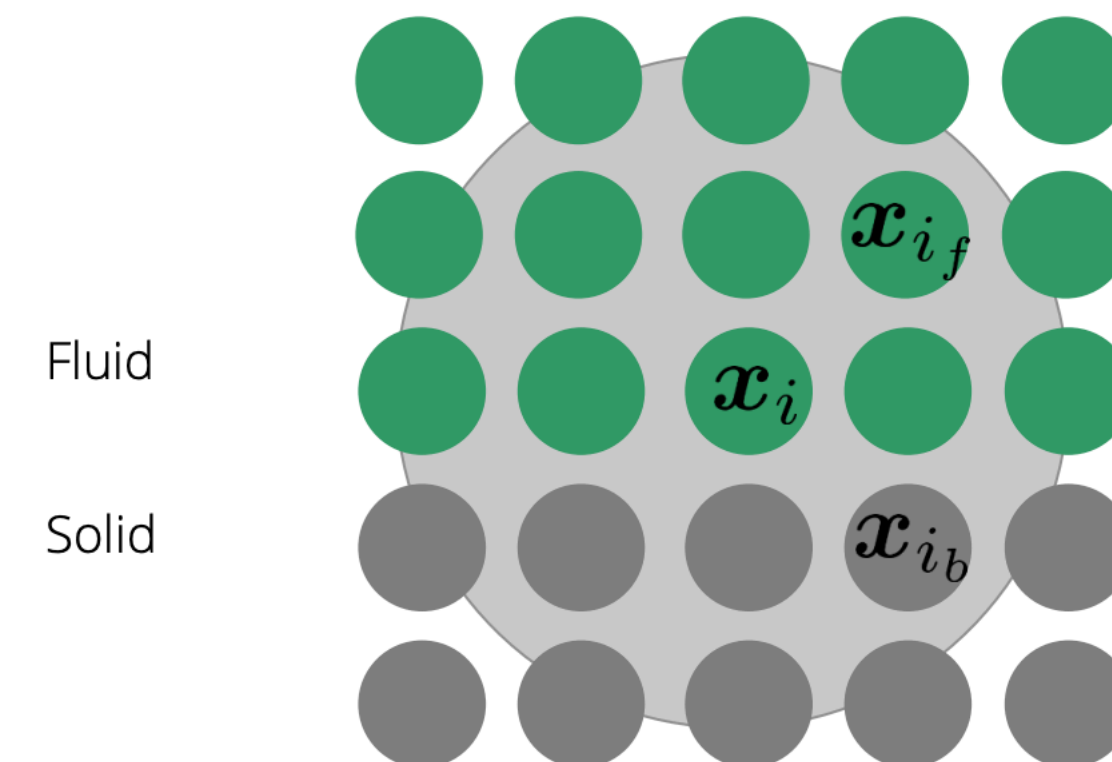
$$\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \nabla \vec{u} + \frac{1}{\rho} \nabla p = \vec{g} + \nu \nabla \cdot \nabla \vec{u},$$
$$\nabla \cdot \vec{u} = 0.$$

Just need to approximate the differential operators,
And relate velocity to pressure via constitutive models

CFL condition: $\Delta t \leq \lambda \frac{\tilde{h}}{\|\mathbf{v}^{\max}\|}$

- All particles are only allowed to move less than the particle diameter per time step for $\lambda = 1$

Use ghost particles to represent solids/air:



This also avoids density underestimation.

Demo!

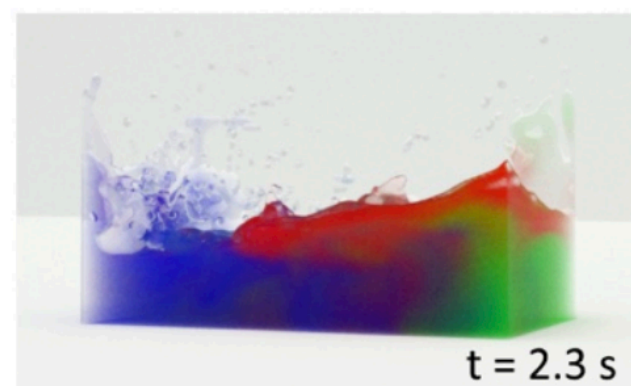
interactivecomputergraphics.github.io/physics-simulation

More on SPH



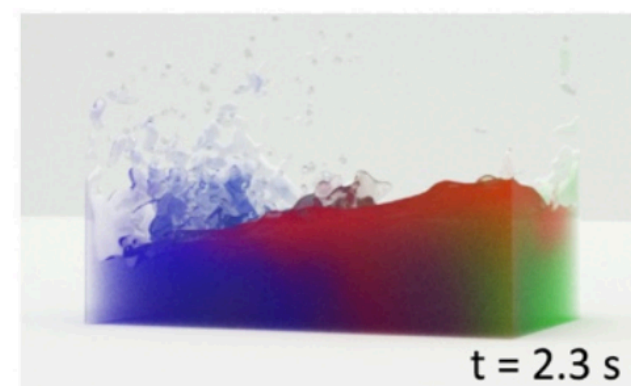
Optimization-based SPH [Xie et al. 2023]

diffusion disabled

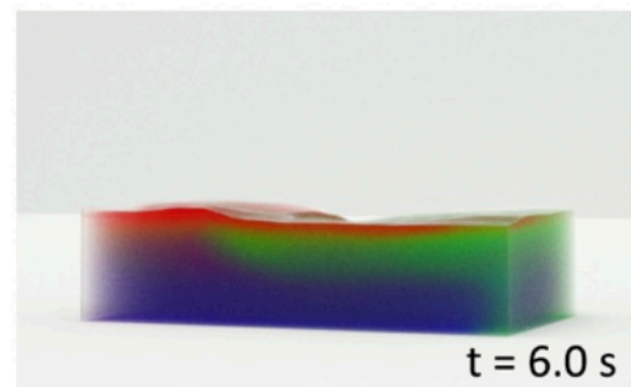


t = 2.3 s

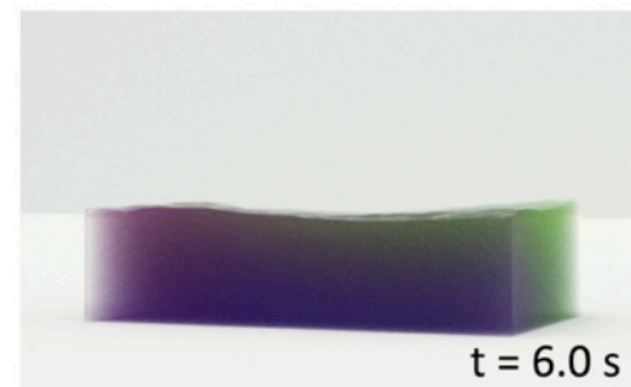
diffusion enabled



t = 2.3 s



t = 6.0 s



t = 6.0 s

Multiphase Fluids [Ren et al. 2014]

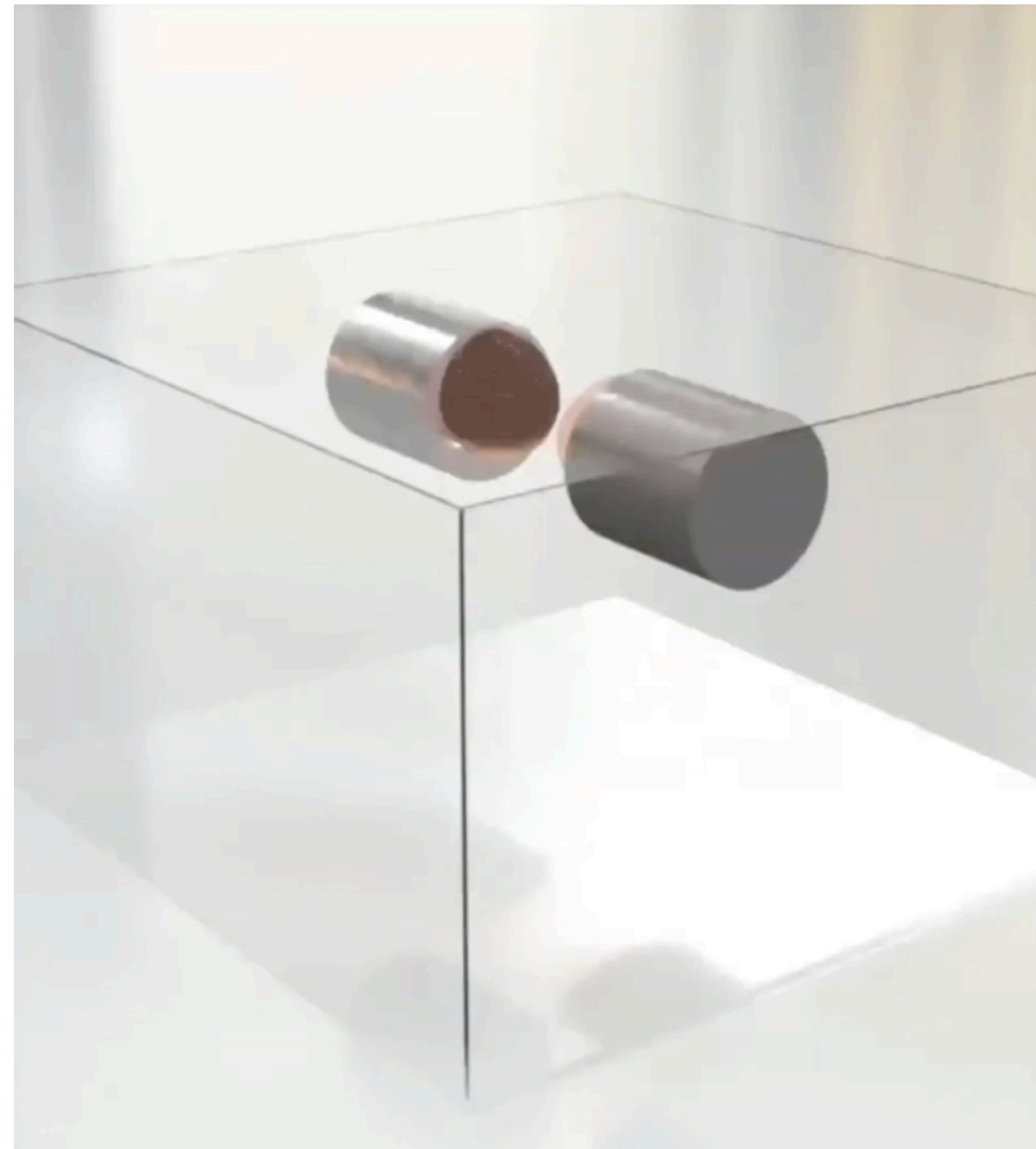
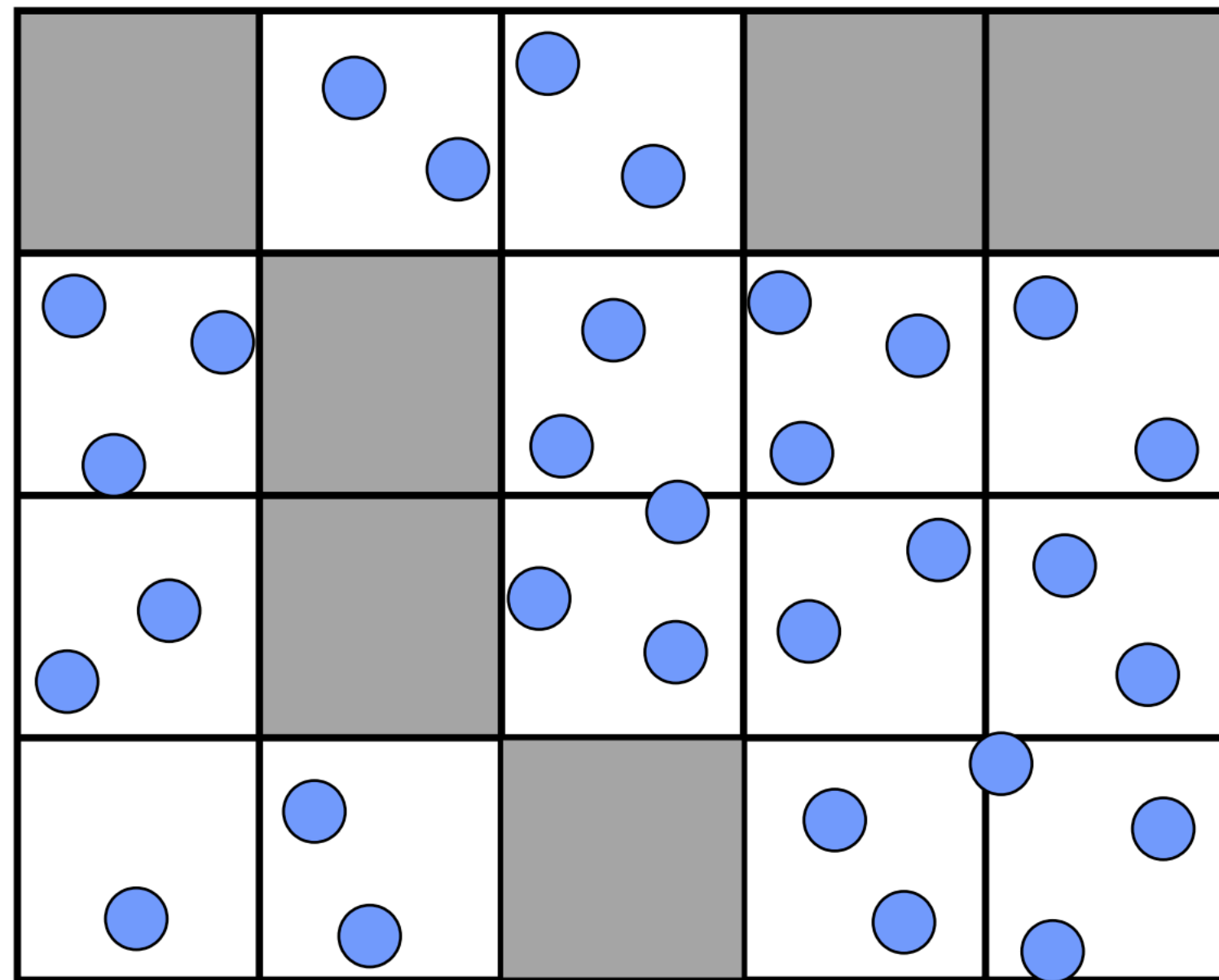
$$\rho \frac{D\mathbf{v}}{Dt} = -\nabla p + \mu_t \nabla \times \boldsymbol{\omega} + \mathbf{f}$$
$$\rho \Theta \frac{D\boldsymbol{\omega}}{Dt} = \mu_t (\nabla \times \mathbf{v} - 2\boldsymbol{\omega}) + \boldsymbol{\tau}$$

Micropolar SPH [Bender et al. 2017]
(particle with self-rotation)



SPH solids [Peer et al. 2018]

Next Lecture: Hybrid Lagrangian/Eulerian Methods



Next Week

- Nov 14: Paper Presentation
 - Chen et al. SIERE: A Hybrid Semi-Implicit Exponential Integrator for Efficiently Simulating Stiff Deformable Objects. ToG 2020 (Presenter: **Kevin You**)
 - Wolper et al. CD-MPM: Continuum Damage Material Point Methods for Dynamic Fracture Animation. SIGGRAPH 2018 (Presenter: **Shilin Ma**)
- Nov 16: Paper Presentation
 - Sharp et al. Data-Free Learning of Reduced-Order Kinematics. SIGGRAPH 2023 (Presenter: **Zoë Marschner**)
 - Sperl et al. Homogenized Yarn-Level Cloth. SIGGRAPH 2020 (Presenter: **Sarah Di**)

Image Sources

- <http://multires.caltech.edu/pubs/ds.pdf>
- <https://www.youtube.com/watch?v=UDQaw4Ff3sg>
- https://en.wikipedia.org/wiki/Smoothed-particle_hydrodynamics
- <https://sph-tutorial.physics-simulation.org/>