

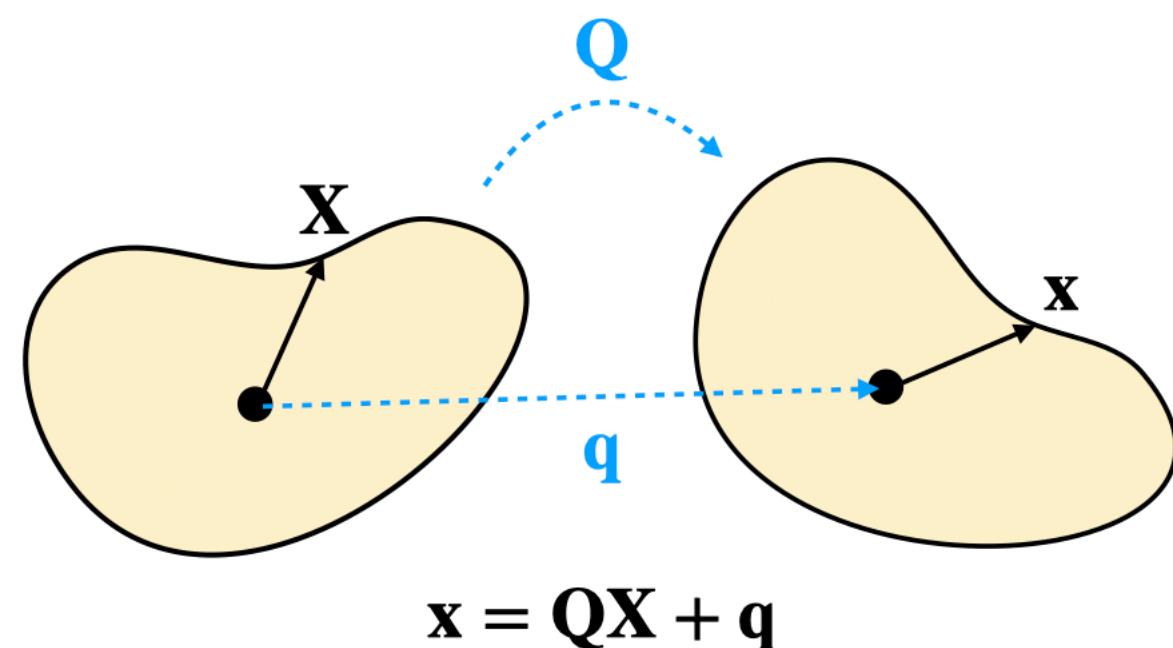
Instructor: Minchen Li



Lec 13: Codimensional Solids

15-763: Physics-based Animation of Solids and Fluids (S25)

Recap: Rigid Body Dynamics



Reduced order DOF:

$$x = QX + q \in \mathbb{R}^3$$

$$x = \bar{X}Q + \bar{S}q \in \mathbb{R}^{3n}$$

$$Q \in \mathbb{R}^{9m}, \bar{X} \in \mathbb{R}^{3n \times 9m}$$

$$q \in \mathbb{R}^{3m}, \bar{S} \in \mathbb{R}^{3n \times 3m}$$

Reduced order dynamics (from subspace optimization):

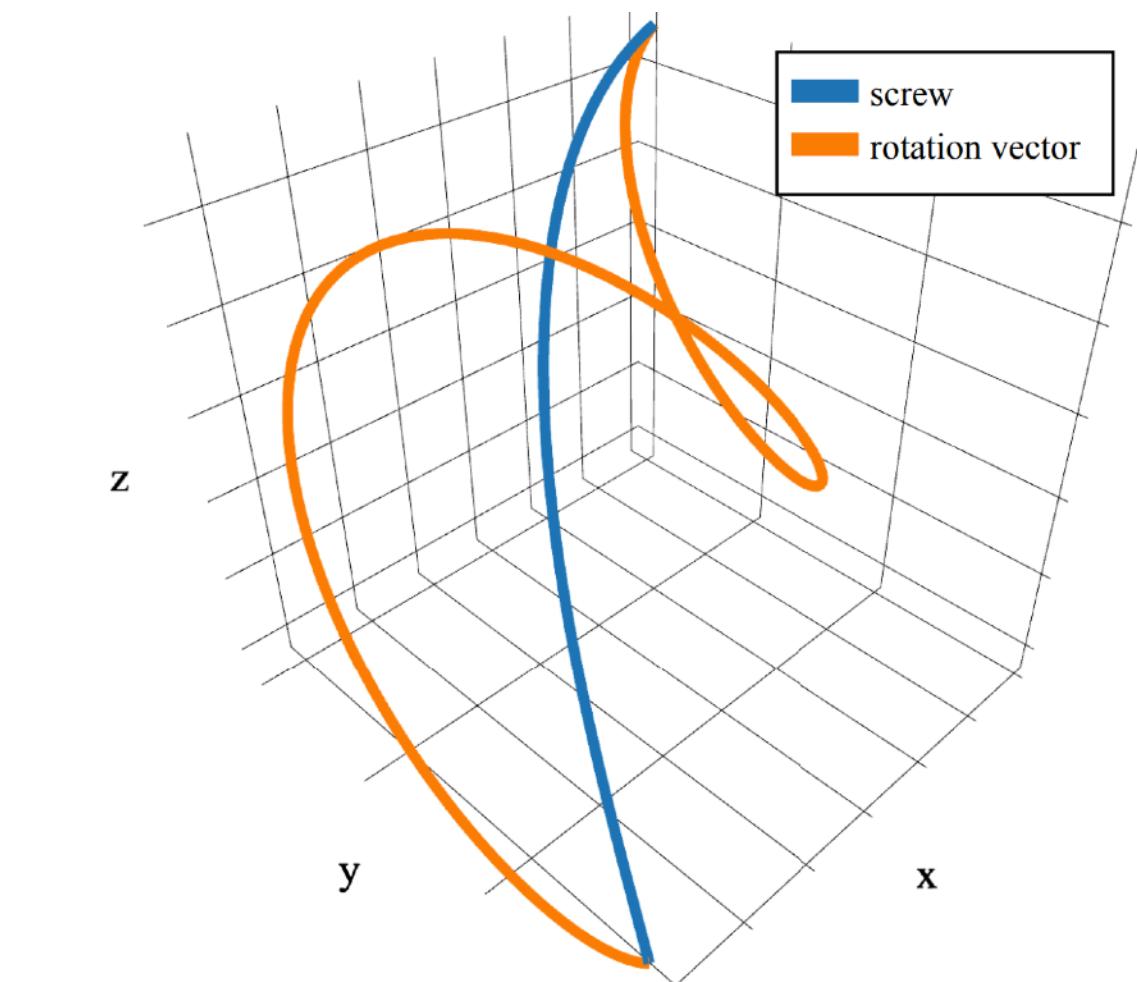
$$\min_{\theta, q} \frac{1}{2} \|\bar{X}R(\theta) + \bar{S}q - \tilde{x}^n\|_M^2 + h^2 \sum P(\bar{X}R(\theta) + \bar{S}q)$$

Rodrigues' Rotation Formula:

$$\mathcal{R}(\theta) = \text{Id} + \sin(\|\theta\|) \left[\frac{\theta}{\|\theta\|} \right] + (1 - \cos(\|\theta\|)) \left[\frac{\theta}{\|\theta\|} \right]^2$$

Just include IPC energies here

CCD is on nonlinear trajectories:



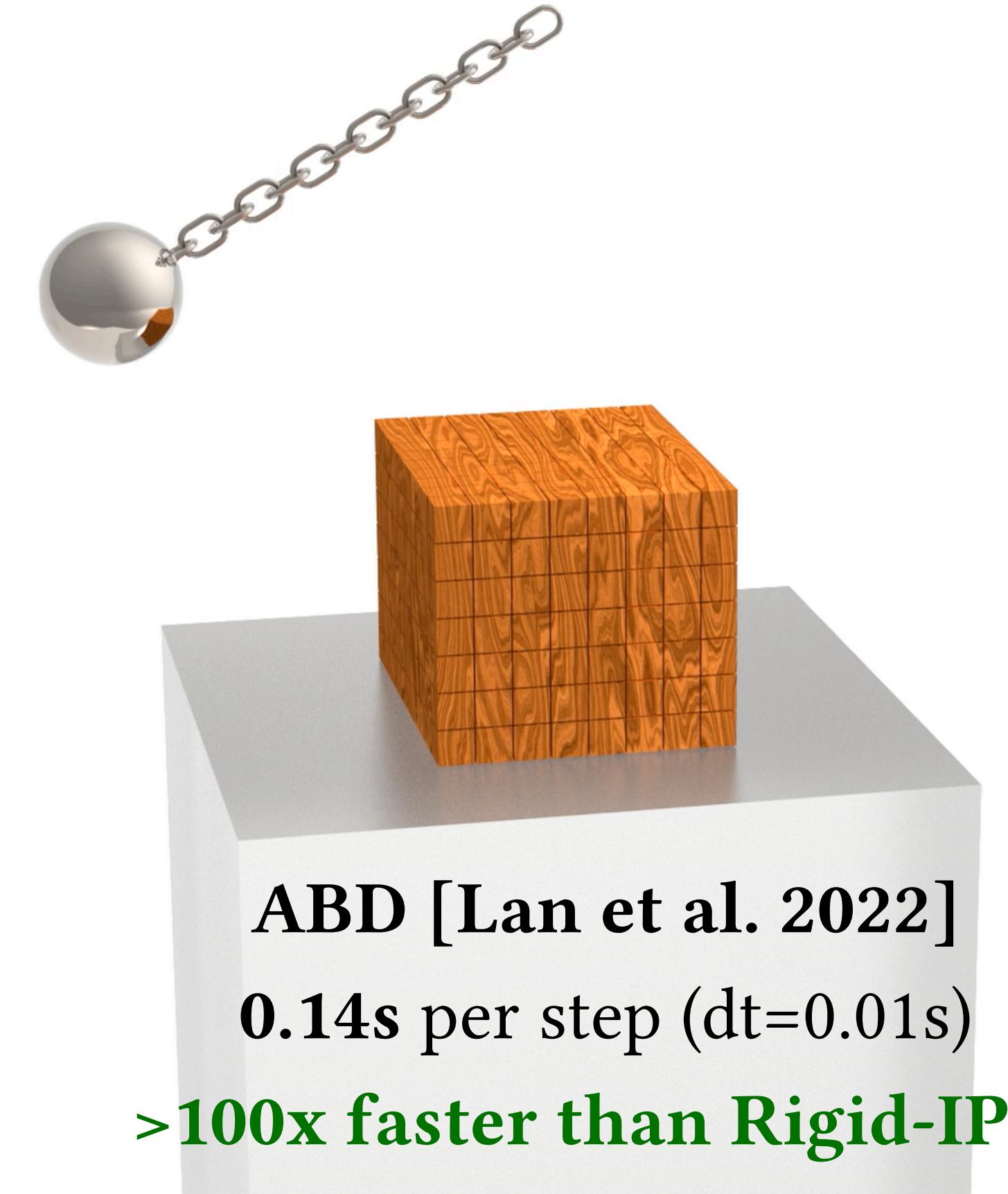
Very expensive!

Recap: Affine Body Dynamics (ABD)

Reduced order dynamics with penalty method:

$$\min_{Q,q} \frac{1}{2} \|\bar{X}Q + \bar{S}q - \tilde{x}^n\|_M^2 + h^2 \sum P(\bar{X}Q + \bar{S}q)$$

Use elasticity with large
Young's modulus



12 DOF per body, still significantly reduced

$x = \bar{X}Q + \bar{S}q$ is linear w.r.t. both Q and q -> linear CCD

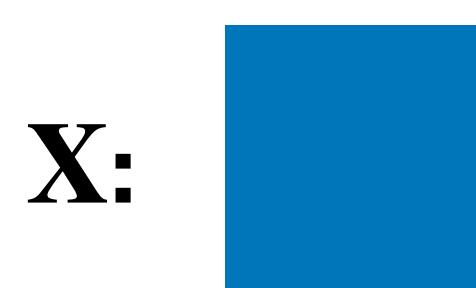
A stiff Ψ won't make the problem harder with stiff IPC energies

Recap: ABD in Another Perspective

Affine Deformation Modes

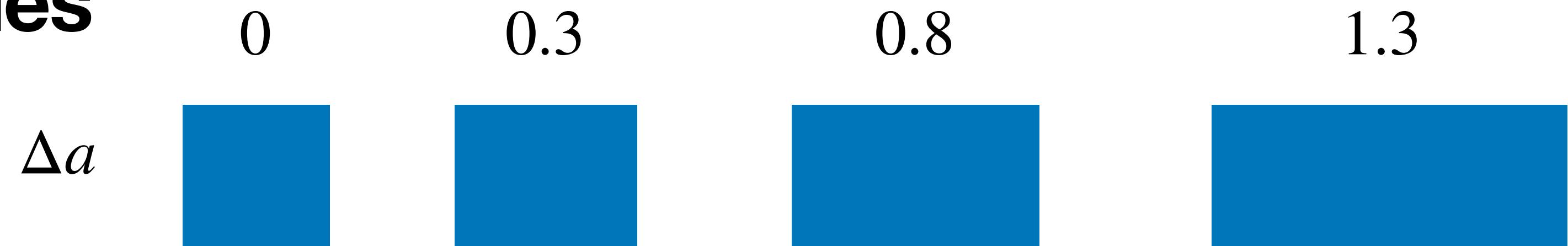
$$\mathbf{x} = \begin{bmatrix} a & b \\ c & d \end{bmatrix} \mathbf{X} + \begin{bmatrix} e \\ f \end{bmatrix}$$

DOF: a, b, c, d, e, f



$$\mathbf{x} = A \begin{bmatrix} a \\ b \\ c \\ d \\ e \\ f \end{bmatrix} = aA_1 + bA_2 + \dots$$

Deformation modes (linearly independent displacement fields)

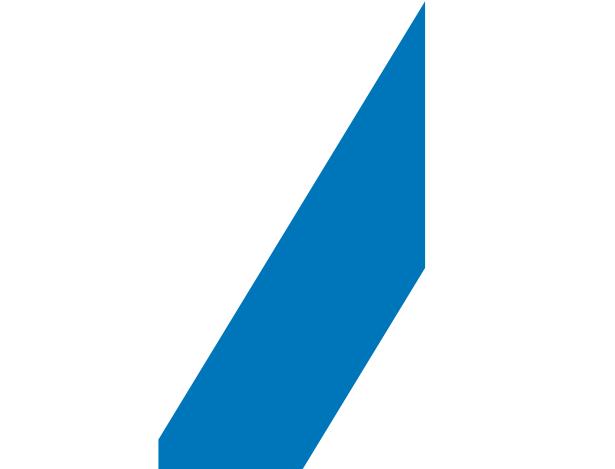
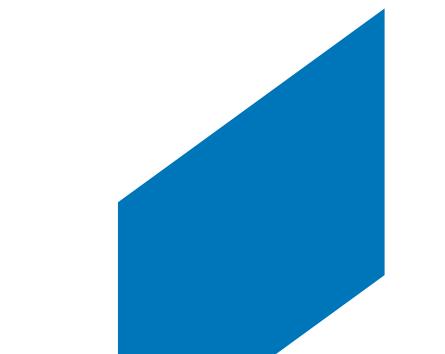


Δd

Δb

Δc

$\mathbf{x}:$



Recap: Reduced Order Model

Linear Modal Analysis

Assume linear elasticity problem: $M\ddot{u} + Ku = f$ s.t. $Sx = 0$ (Dirichlet BC)

Intuition: Meaningful deformation modes are those don't generate large forces

Can solve the generalized Eigenvalue problem to find them: $\bar{K}y = \lambda \bar{M}y$

(where \bar{K} and \bar{M} do not account for BC nodes)

(Take the Eigenvectors with smallest Eigenvalues as modes.)

Let $u = x - X = Uz$, where $z \in \mathbb{R}^k$ are the reduced DOF, $U \in \mathbb{R}^{3n \times k}$ formed by the Eigenvectors,

Plugging in $M\ddot{u} + Ku = f$, ignoring BCs for now: $\ddot{z} + \Lambda z = U^T f$ **Diagonal system! Super fast!**

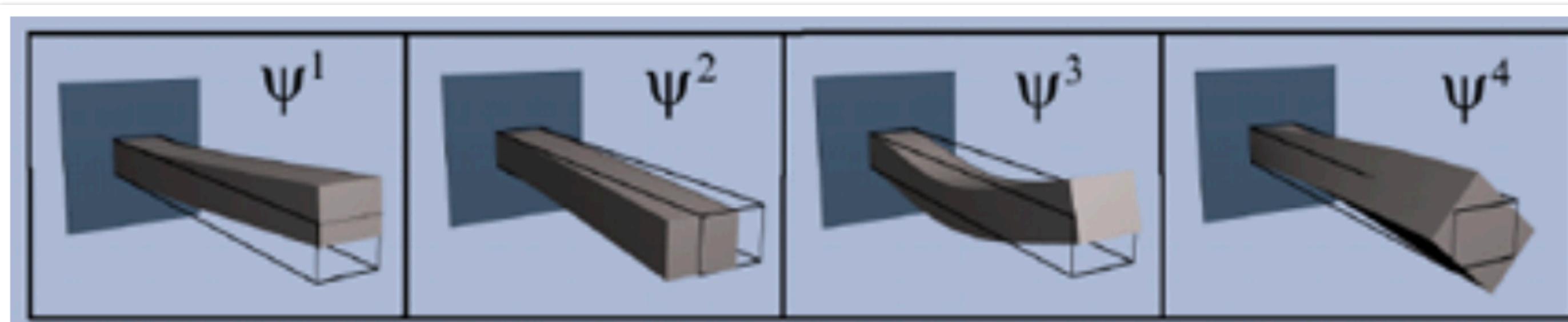


Figure 2: Linear modes for a cantilever beam.

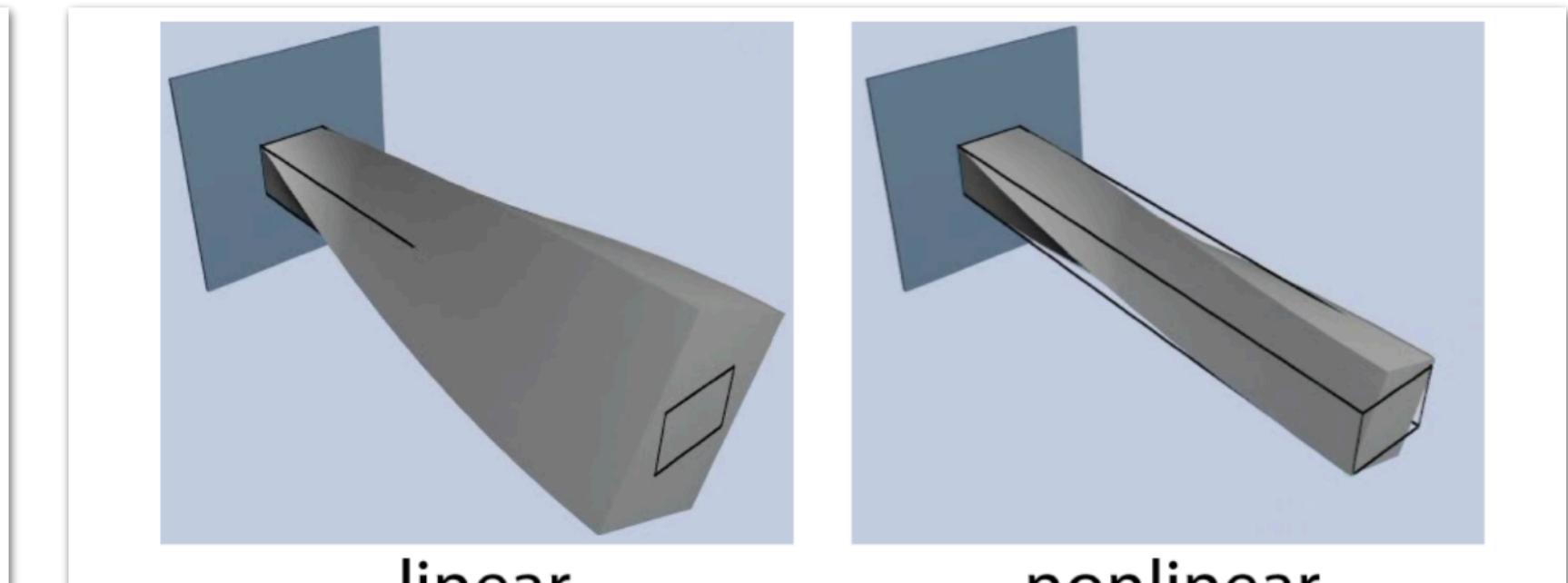


Figure 3: Model reduction applied to a linear and nonlinear system.

Recap: Reduced Order Model

Nonlinear Elasticity

Plugging in $u = Uz$: $\min_z \frac{1}{2} \|X + Uz - \tilde{x}^n\|_M^2 + h^2 \sum P(X + Uz)$

Gradient: $U^T M(X + Uz - \tilde{x}^n) + h^2 \sum U^T \nabla P(X + Uz)$

Hessian: $U^T M U + h^2 \sum U^T \nabla^2 P(X + Uz) U$

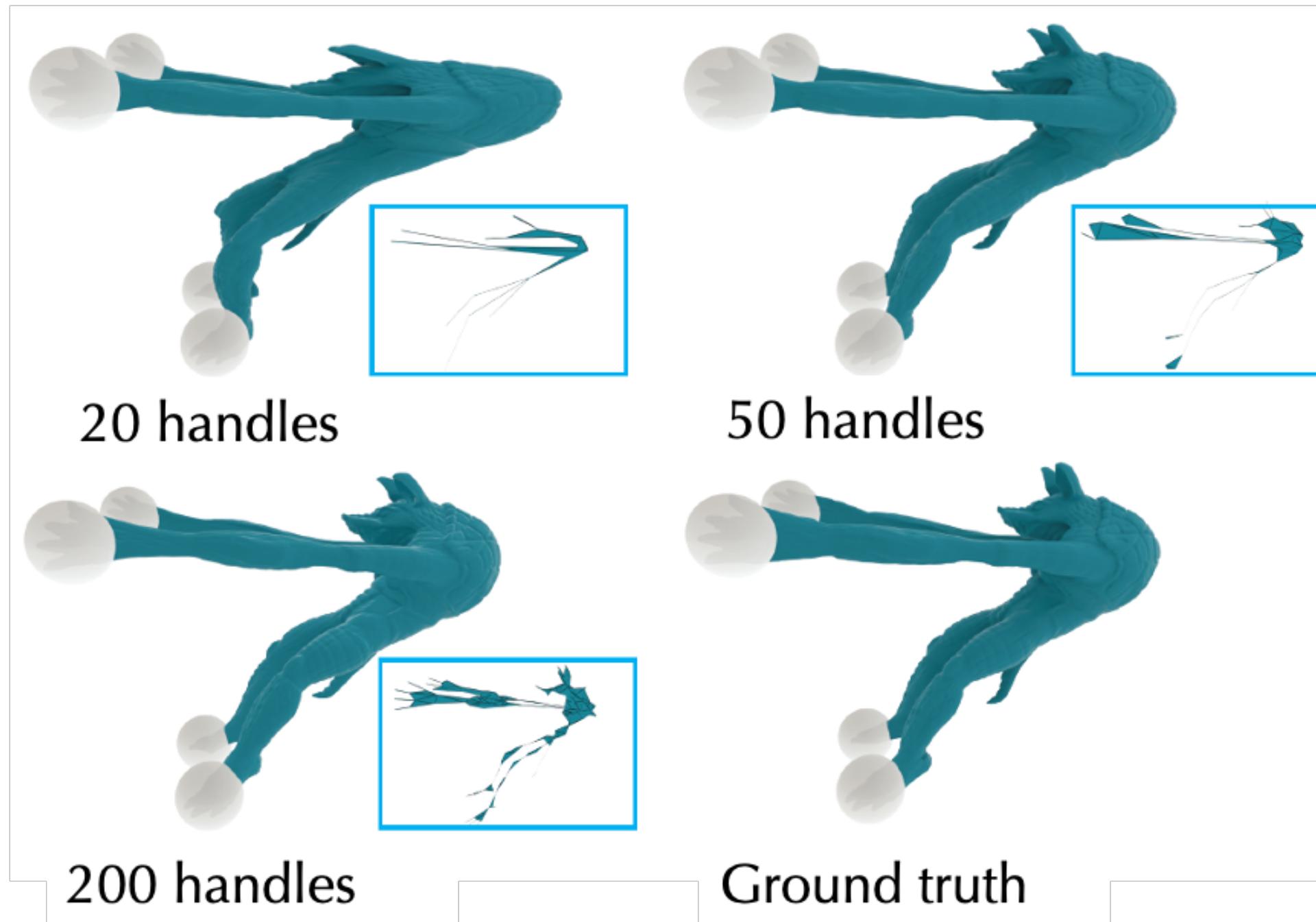
Can use numerical integration to approximate Gradient and Hessian, minimizing the number of quadratures [An et al. 2008]

To design better deformation modes:

- Use locally supported modes for sparsity, e.g. **Medial Axis Mesh** [Lan et al. 2021]
- Use simulated poses/deformed configurations as data, and perform PCA
- Use modal derivatives to construct a quadratic function $u = f(z)$ [∗]
- Use neural networks to learn $u = f(z)$

Results: Reduced Simulation of Deformable Solids

Medial IPC [Lan et al. 2021]



Puffer Ball x 1
36× speedup

of Handles: 1624
of Elements: 625k



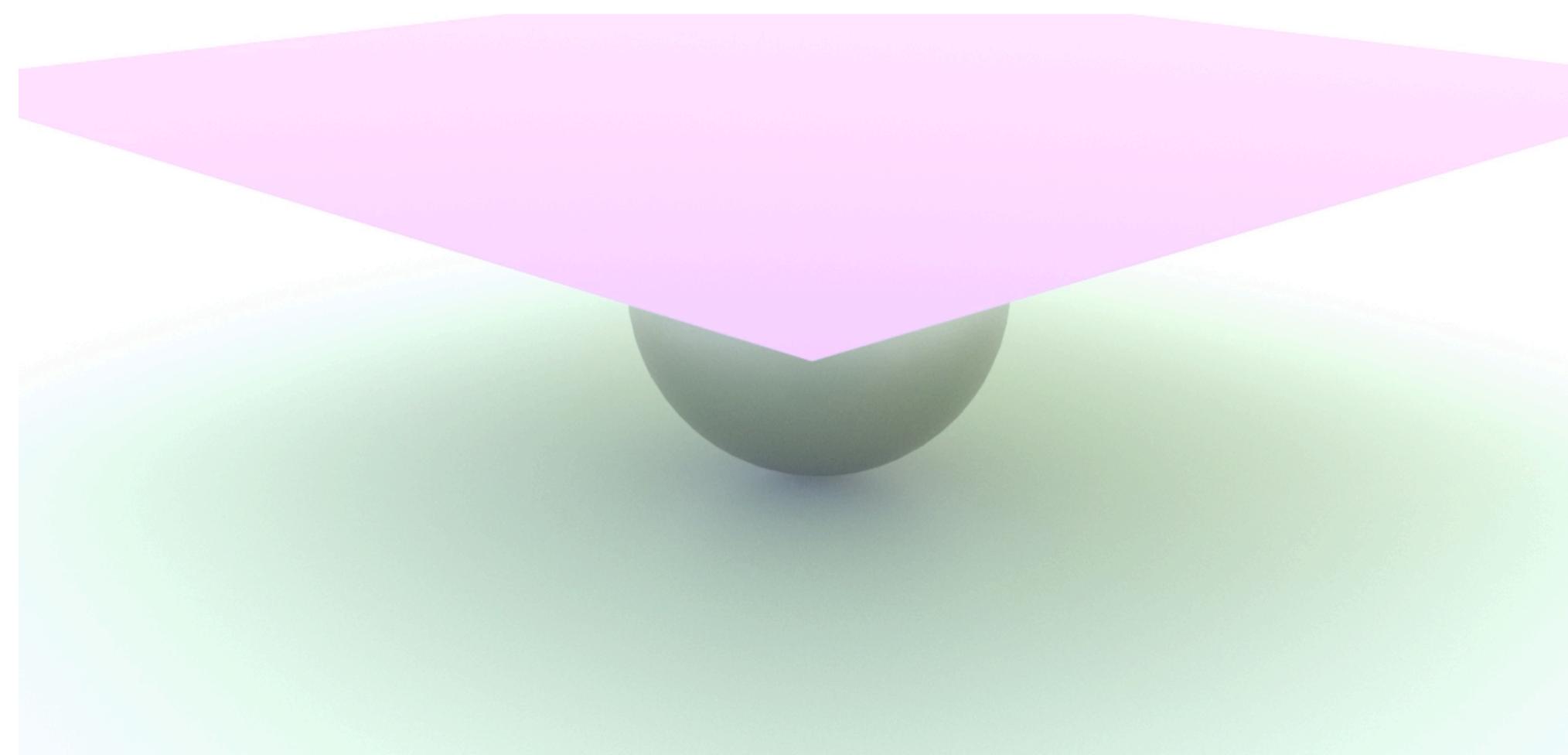
Topics Today:

- Thin Shells
 - ▶ Stretching and Bending
 - ▶ Strain Limiting and Thickness
- Rods and Particles

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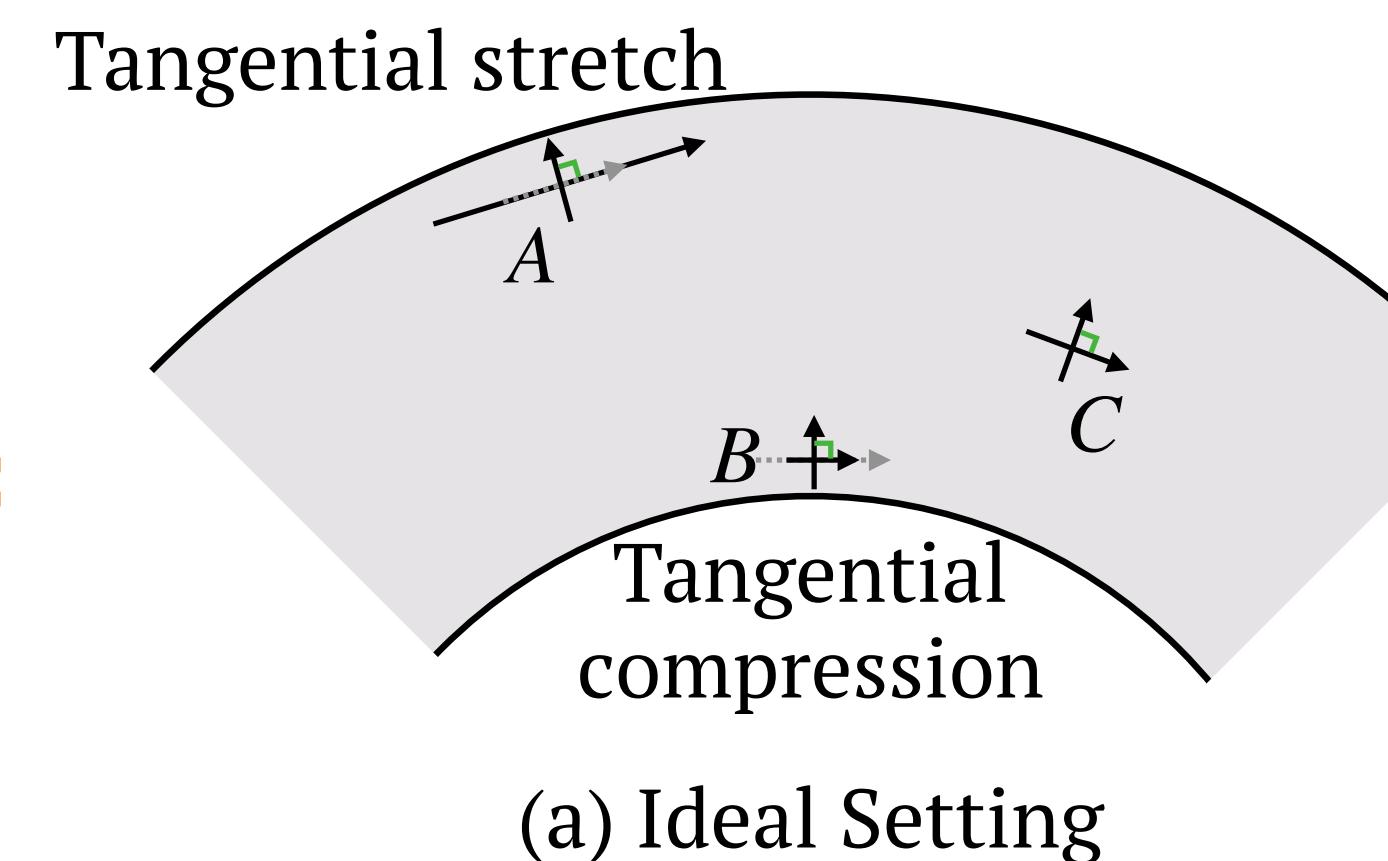
- **Thin Shells**
 - ▶ **Stretching and Bending**
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Simulating Thin Objects Using Volumetric Meshes?

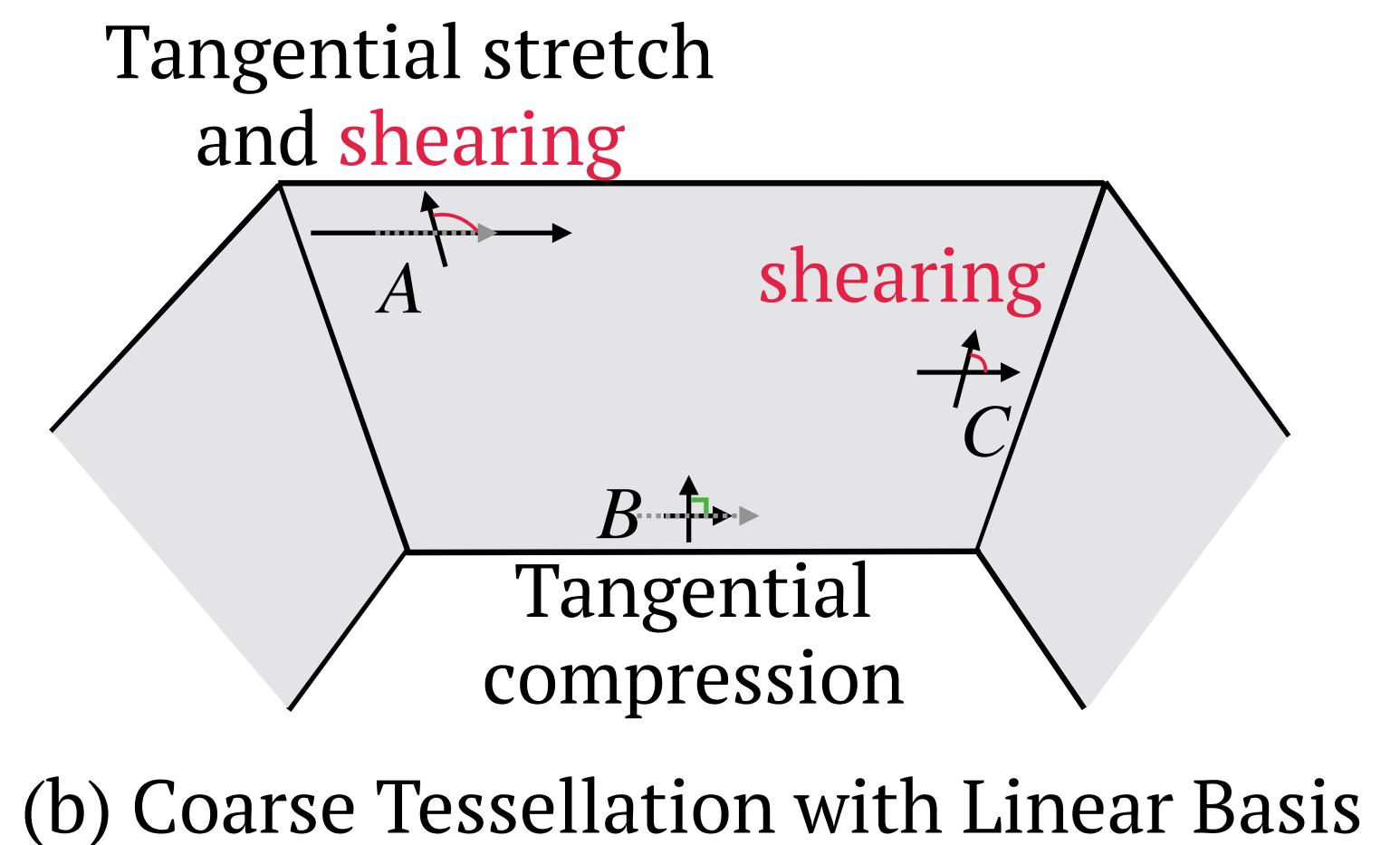


**Shear locking issue
(linear shape functions):**

**Higher-order shape
functions are expensive**



III-conditioning:



Simulating Thin Shells using Surface Meshes

Tangent Space Elasticity

Thickness is tiny and barely visible -> can ignore it: 

Use surface meshes, e.g. triangle meshes, to simulate thin shells, e.g. cloth, paper, etc

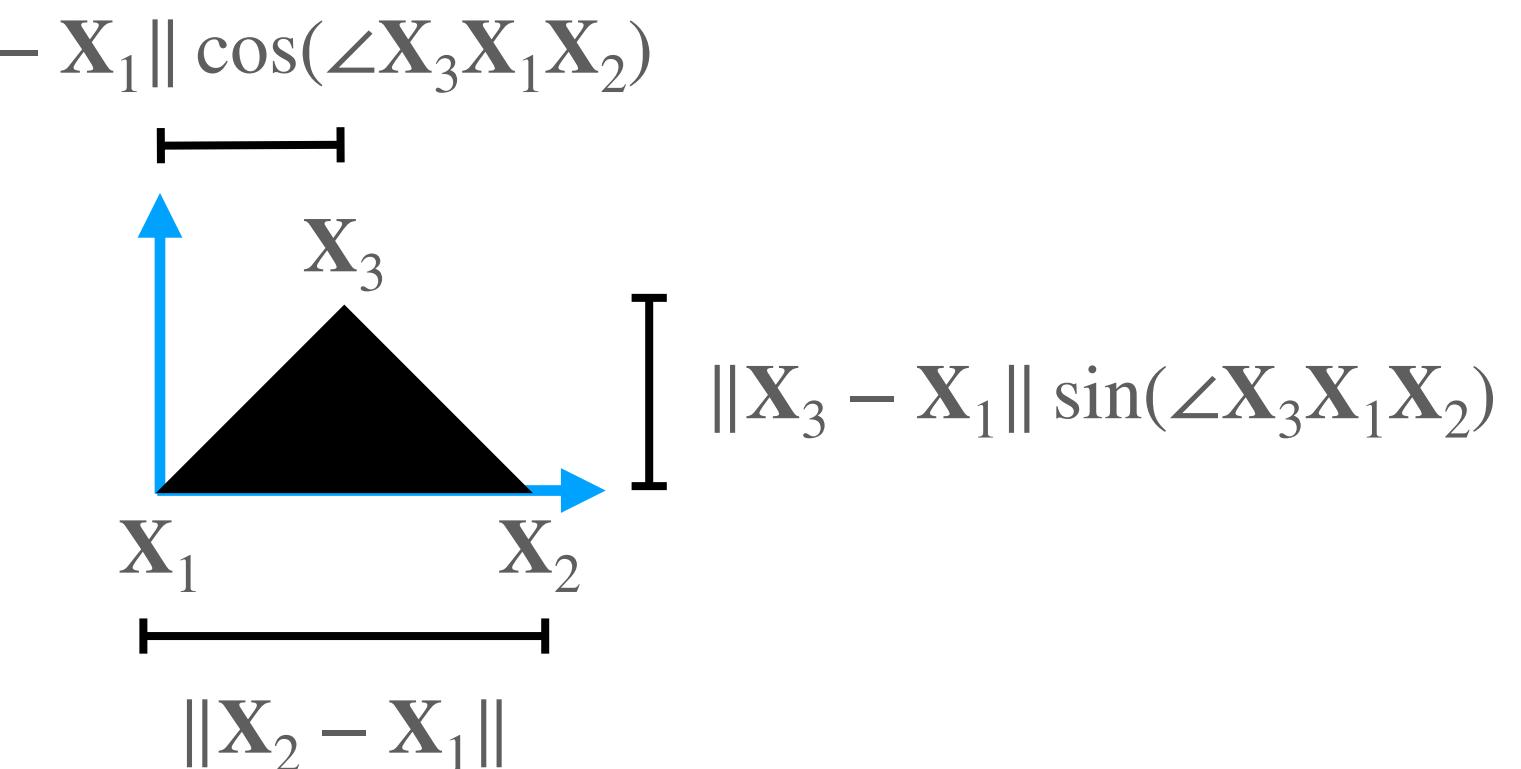
$$F = \begin{bmatrix} x_2 - x_1, x_3 - x_1 \end{bmatrix} \begin{bmatrix} \|X_2 - X_1\| & \frac{(X_3 - X_1) \cdot (X_2 - X_1)}{\|X_2 - X_1\|} \\ 0 & \frac{\|(X_3 - X_1) \times (X_2 - X_1)\|}{\|X_2 - X_1\|} \end{bmatrix}^{-1} \in R^{3 \times 2}$$

$$\mathbf{F} = \mathbf{U} \boldsymbol{\Sigma} \mathbf{V}^T \quad \hat{\Psi}_{\text{NH}}(\boldsymbol{\Sigma}) = \frac{\mu}{2} \left(\sum_i^d \sigma_i^2 - d \right) - \mu \ln(J) + \frac{\lambda}{2} \ln^2(J)$$

Lame parameter λ is computed differently here for shells as the thickness approaches zero:

$$\lambda = \frac{E\nu}{1 - \nu^2} \quad \text{(Plane stress approximation)}$$

$$\lambda = \frac{E\nu}{(1 + \nu)(1 - 2\nu)} \quad \text{(Volumetric)}$$



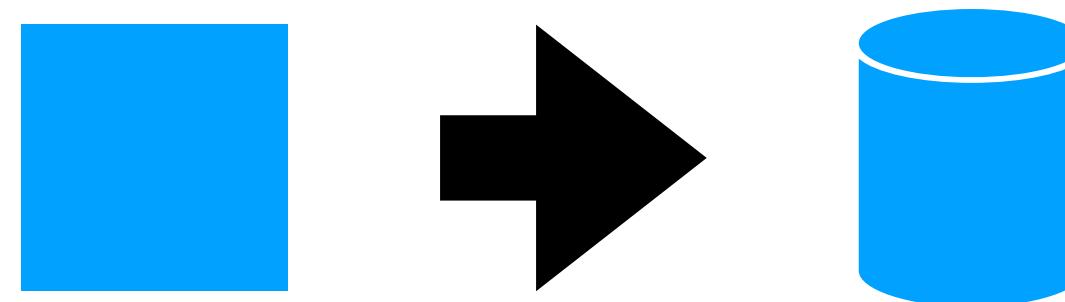
$$\sum_i V_i \Psi(\mathbf{F}_i) \quad V_i = \xi \overline{A}_i \begin{matrix} \text{Thickness} \\ \text{Triangle area} \end{matrix}$$

*May also use The First Fundamental Form to compute Ψ .

Simulating Thin Shells using Surface Meshes

Bending

With only tangent space elasticity, no force under isometric deformation:

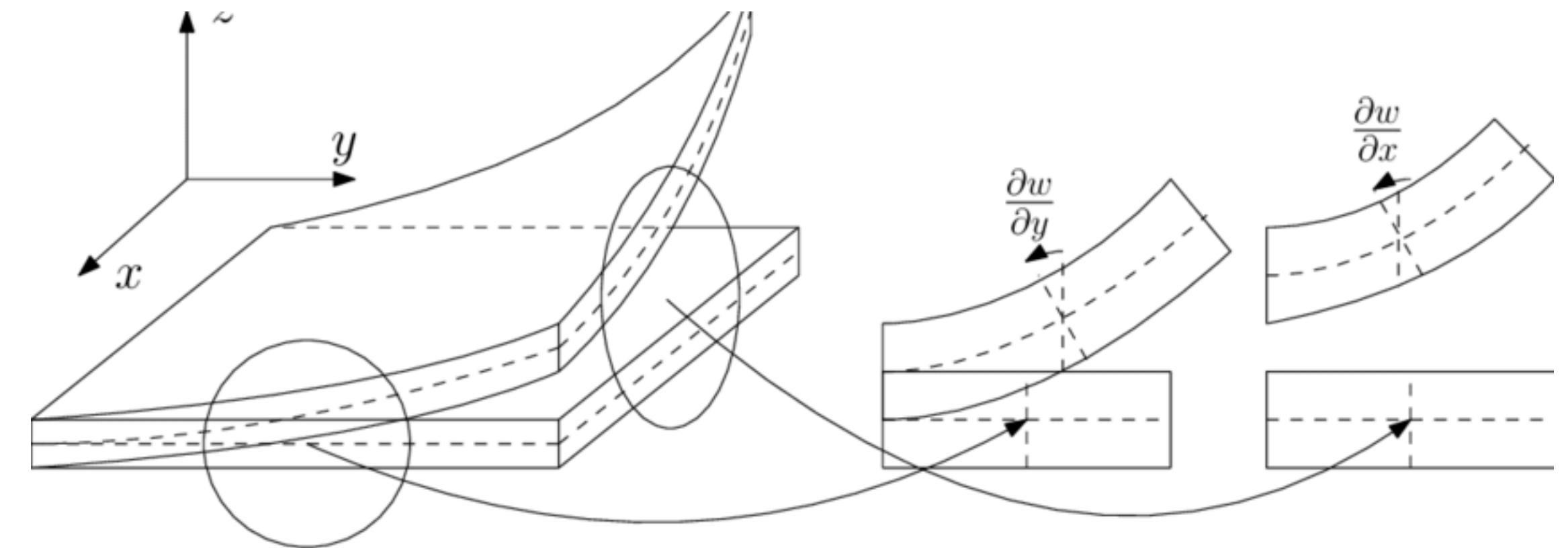


Need to additionally model bending resistance!

The Kirchoff-Love Model

Deriving strain energies for bending from continuum mechanics, based on assumptions:

- straight lines normal to the mid-surface remain straight and normal to the mid-surface after deformation
- the thickness of the plate does not change during a deformation.



Simulating Thin Shells using Surface Meshes

Discrete Shell – Hinge Bending Model [Grinspun et al. 2003]

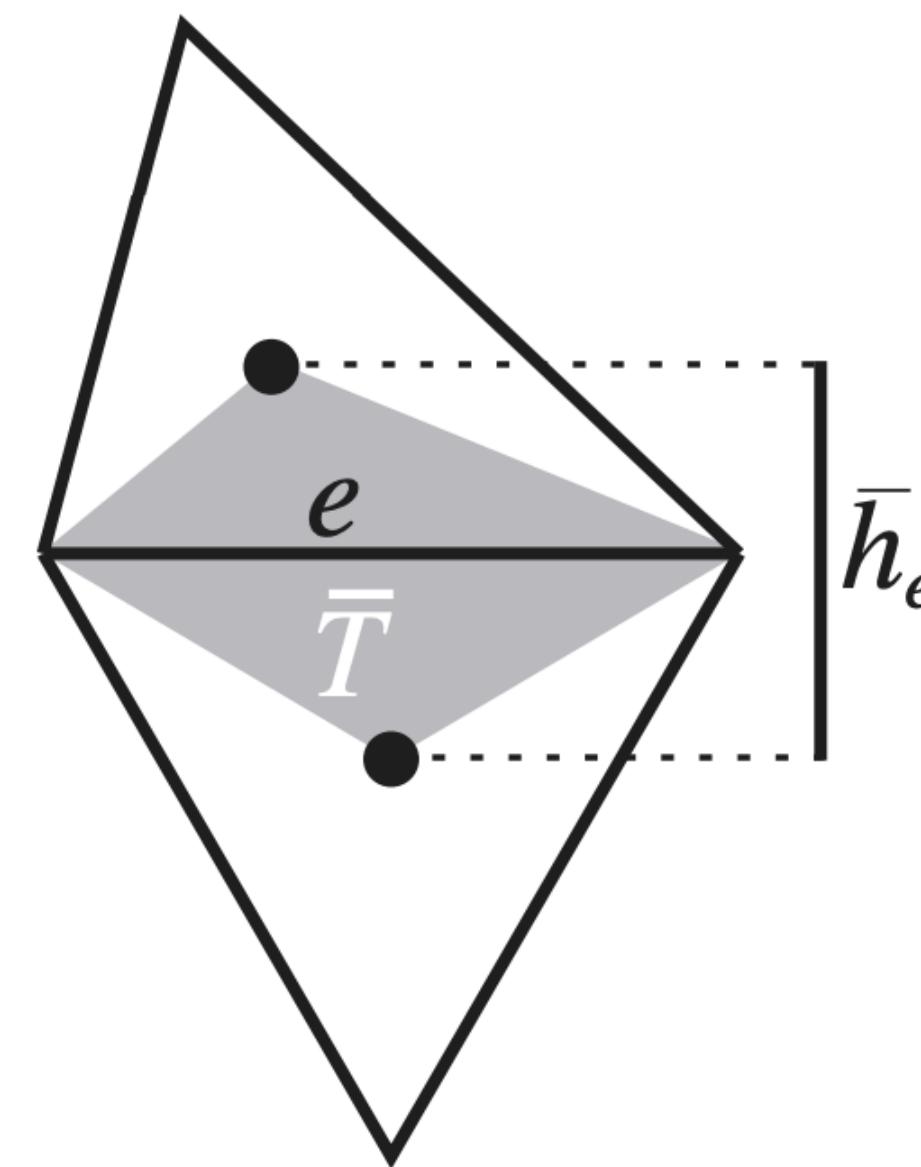
Model the strain energy for bending directly as a penalty of mean curvature changes

$$\int_{\bar{\Omega}} (H \circ \varphi - \bar{H})^2 d\bar{A}$$

Discretizing onto edges of triangle meshes:

$$W_B(\mathbf{x}) = \sum_e (\theta_e - \bar{\theta}_e)^2 \|\bar{e}\| / \bar{h}_e$$

θ is the dihedral angle, which
can be computed with $\arctan()$



Adding stiffness and reparameterize:

$$\Psi_{\text{bend}}(x) = \sum_i k \frac{3\|\bar{e}_i\|^2}{\bar{A}_i} (\theta_i - \bar{\theta}_i)^2$$

$$k = \frac{E\xi^3}{24(1 - \nu^2)}$$

Simulating Thin Shells using Surface Meshes Cubic and Quadratic Bending Energies

Garg et al. [2007]:
For isometric deformation,
A bending energy can be formulated as
a cubic polynomial of x

Bergou et al. [2006]:
For isometric deformation of plates (flat rest shapes),
A bending energy can be formulated as
a quadratic polynomial of x

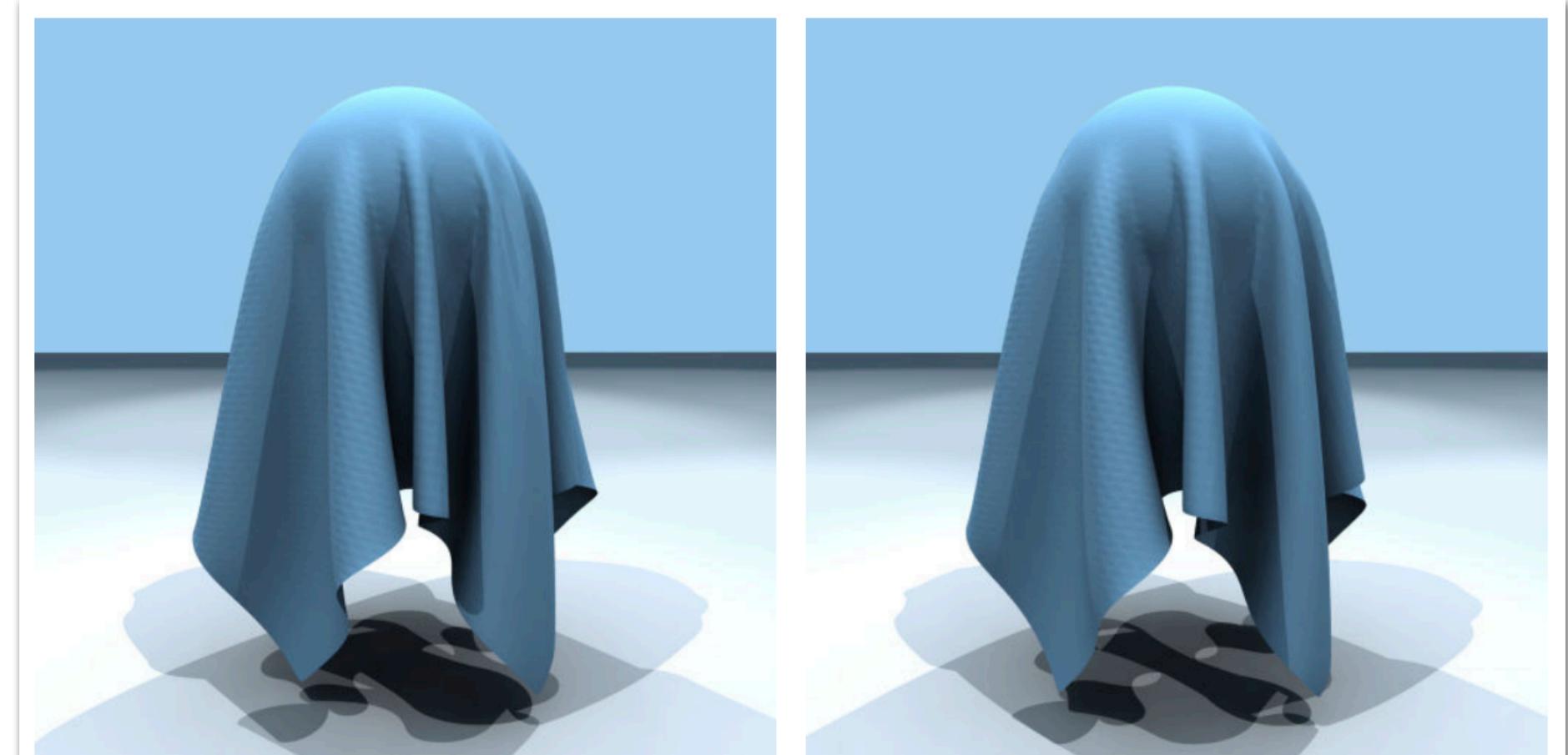


Figure 1: Final rest state of a cloth draped over a sphere, for (left) the proposed isometric bending model and (right) the widely-adopted nonlinear hinge model.

Topics Today:

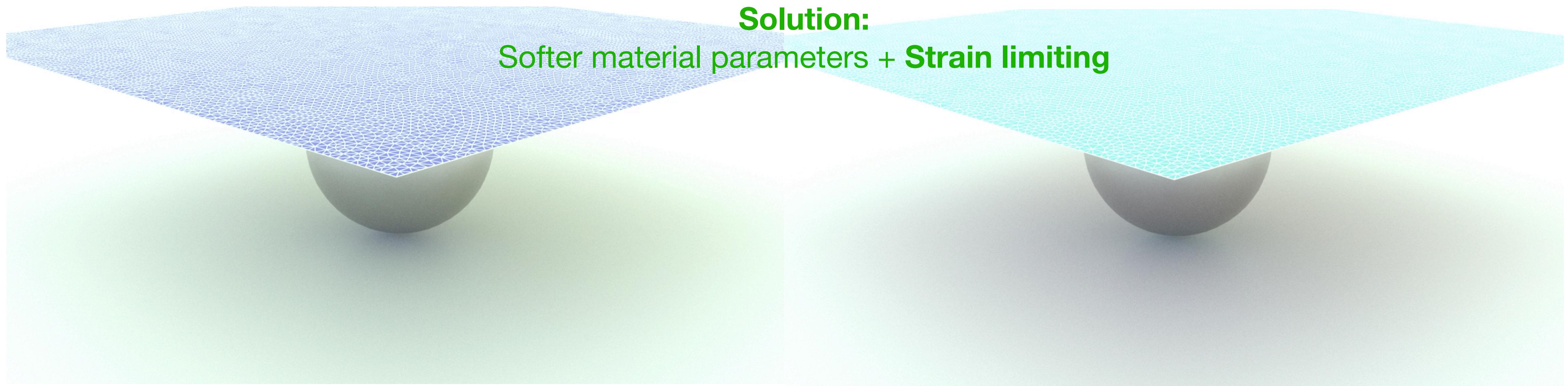
- **Thin Shells**
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Simulating Cloth using Surface Meshes

Membrane Locking

Cloth are nearly **unstretchable** – **stiff stretch resistance, $E = \sim 10^7 \text{ Pa}$**

With low-res triangulation, there can be **geometric lockings**:



Stiff membrane creates extra bending penalty
(real material parameter)

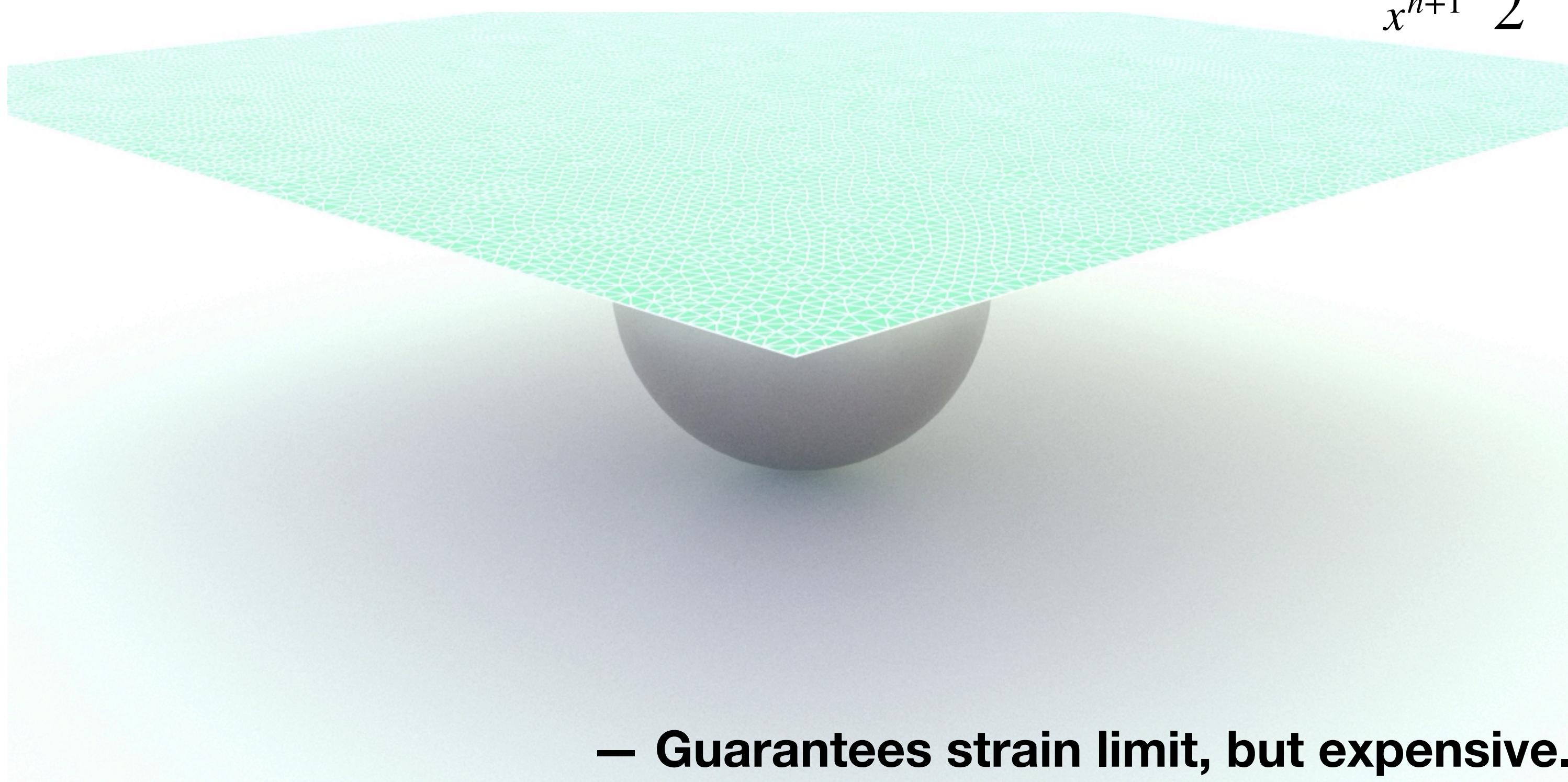
Stretchy artifact
(0.01x real material parameter)

Simulating Cloth using Surface Meshes

Avoiding Membrane Locking with Strain Limiting

$$\forall t, i \quad S_{t,i} < s \quad (F_t = U_t S_t V_t^T \text{ is the SVD of triangle } t \text{'s deformation gradient})$$

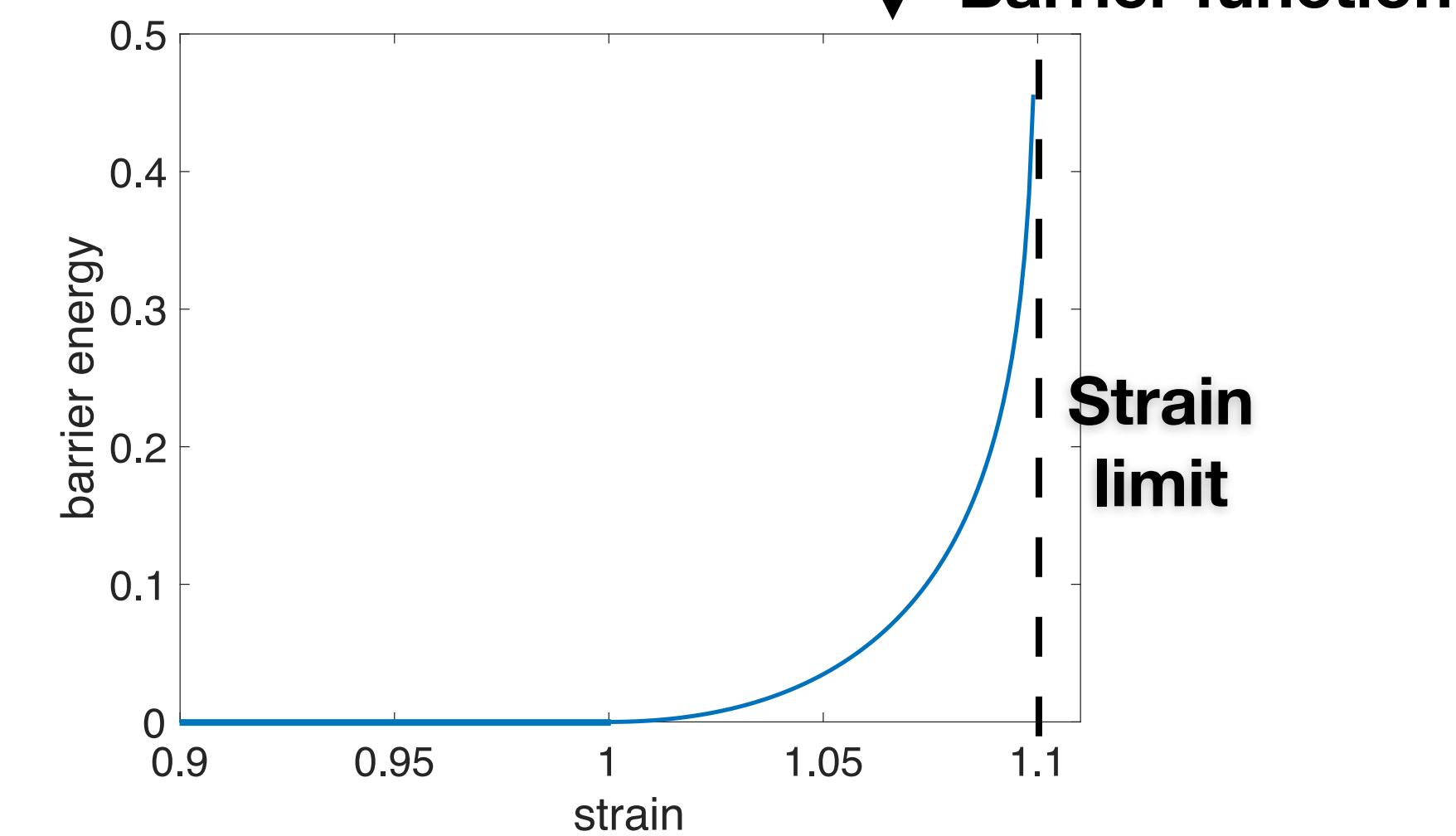
↓
Strain limit



$$\min_{x^{n+1}} \frac{1}{2} \|x^{n+1} - \tilde{x}^n\|_M^2 + h^2(\Psi(x^{n+1}) + B_s(x^{n+1}))$$

$$B_s(x^{n+1}) = \kappa_s \sum_{t,i} \mathcal{V}_t b(S_{t,i}(x^{n+1}))$$

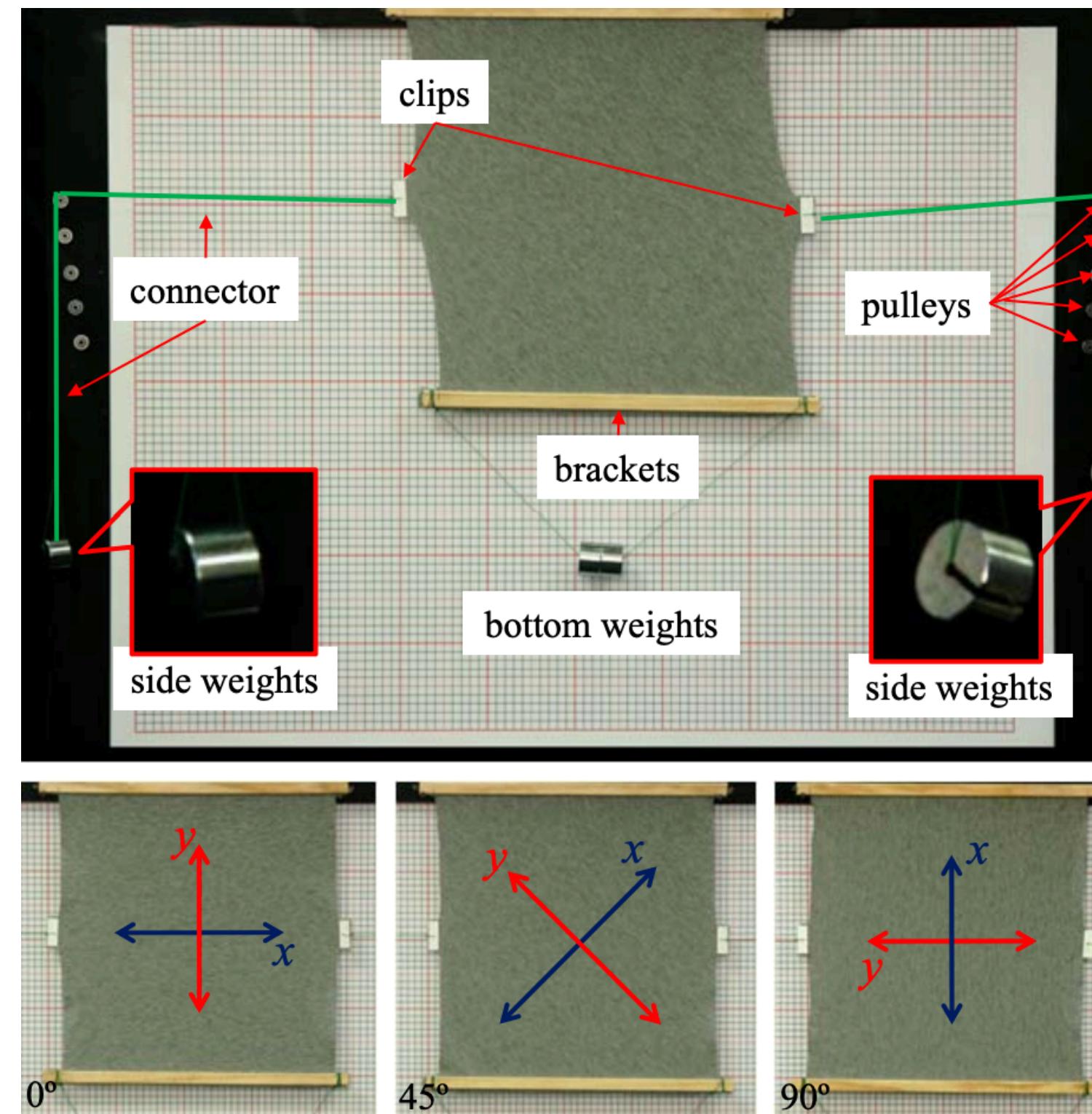
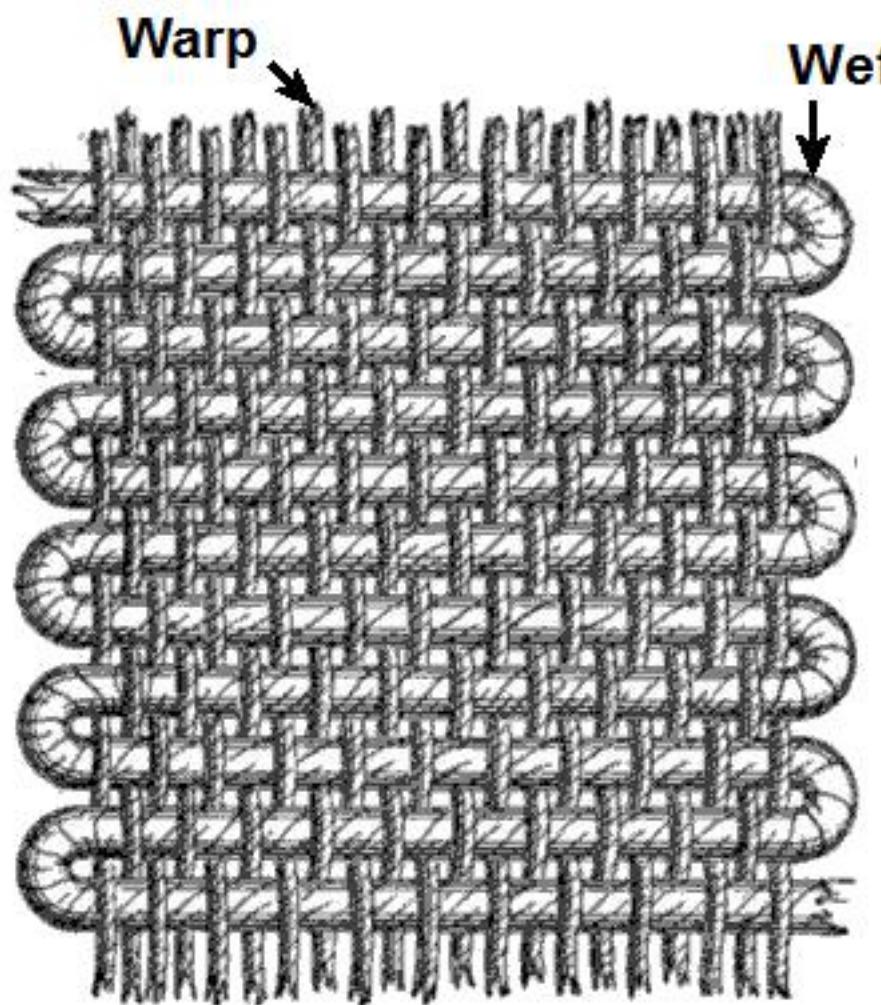
↑
Stiffness
↑
Volume weighting
↓
Barrier function



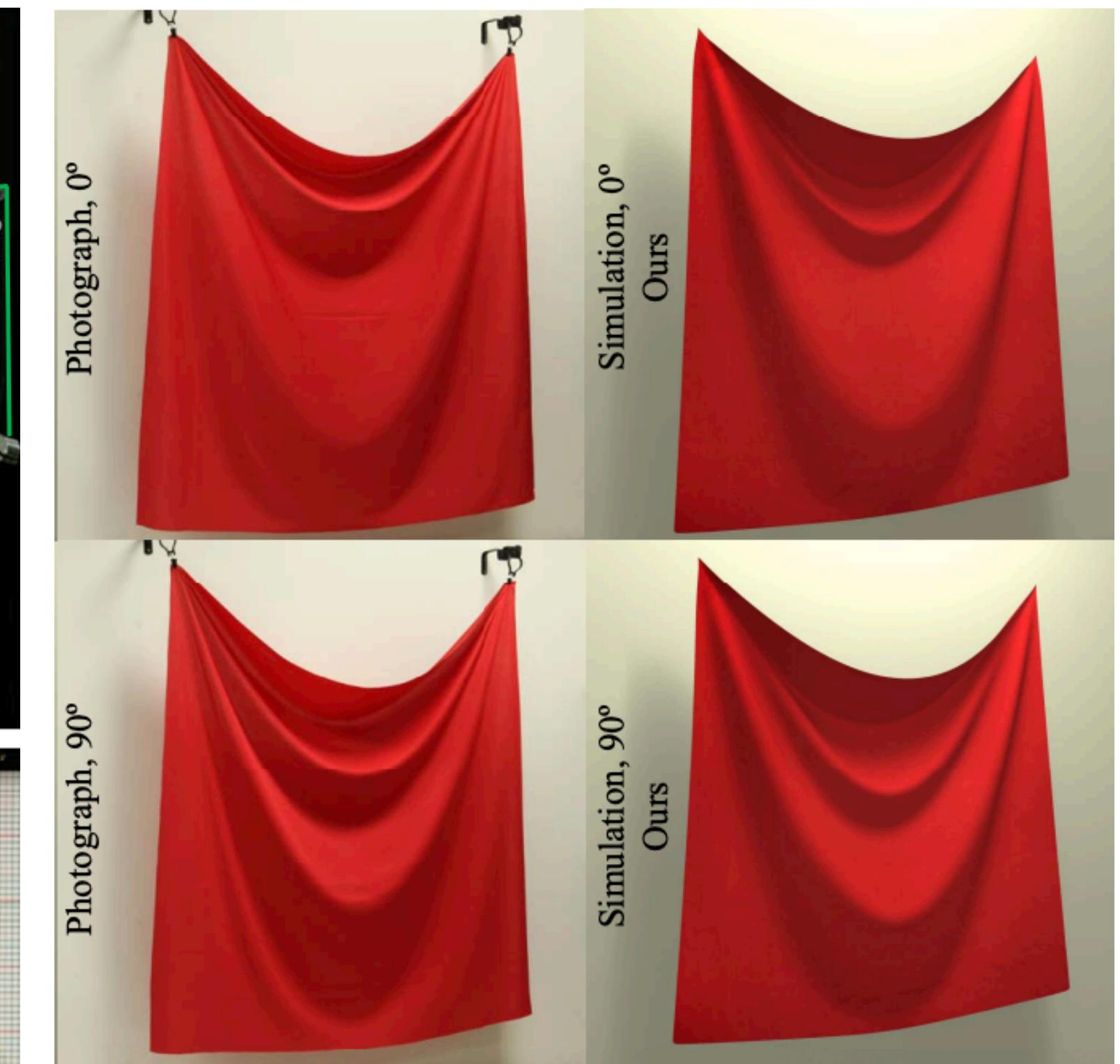
Simulating Cloth using Surface Meshes

Anisotropy

Because of the knitting pattern, cloth is anisotropic



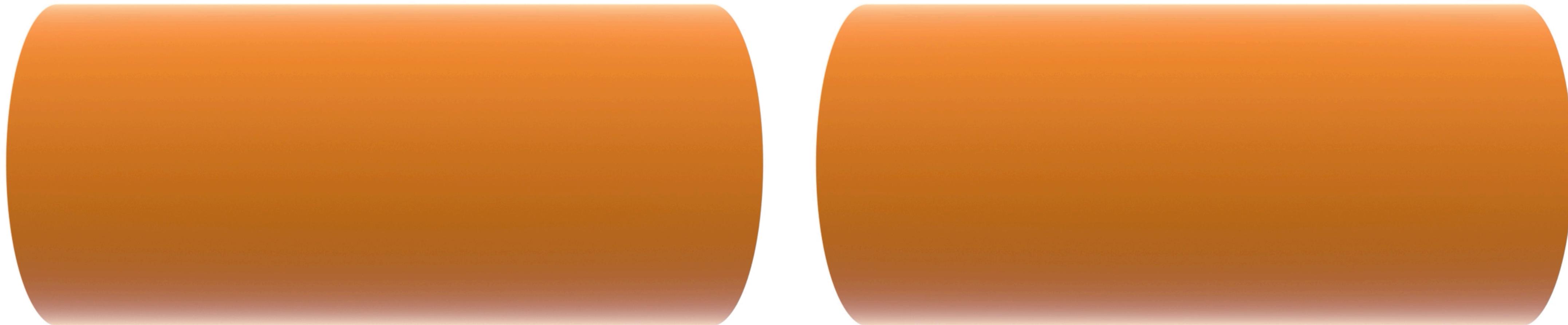
Measuring and simulating cloth based on anisotropic elasticity [Wang et al. 2011]:



Simulating Cloth using Surface Meshes

Thickness Modeling – Inelastic Thickness via Contact Gap

However, there are scenarios where thickness matters:



$$\min_{x^{n+1}} \frac{1}{2} \|x^{n+1} - \tilde{x}^n\|_M^2 + h^2 \sum P(x^{n+1}) + \kappa \sum_k b(D_k(x^{n+1}) - \xi, \hat{d})$$

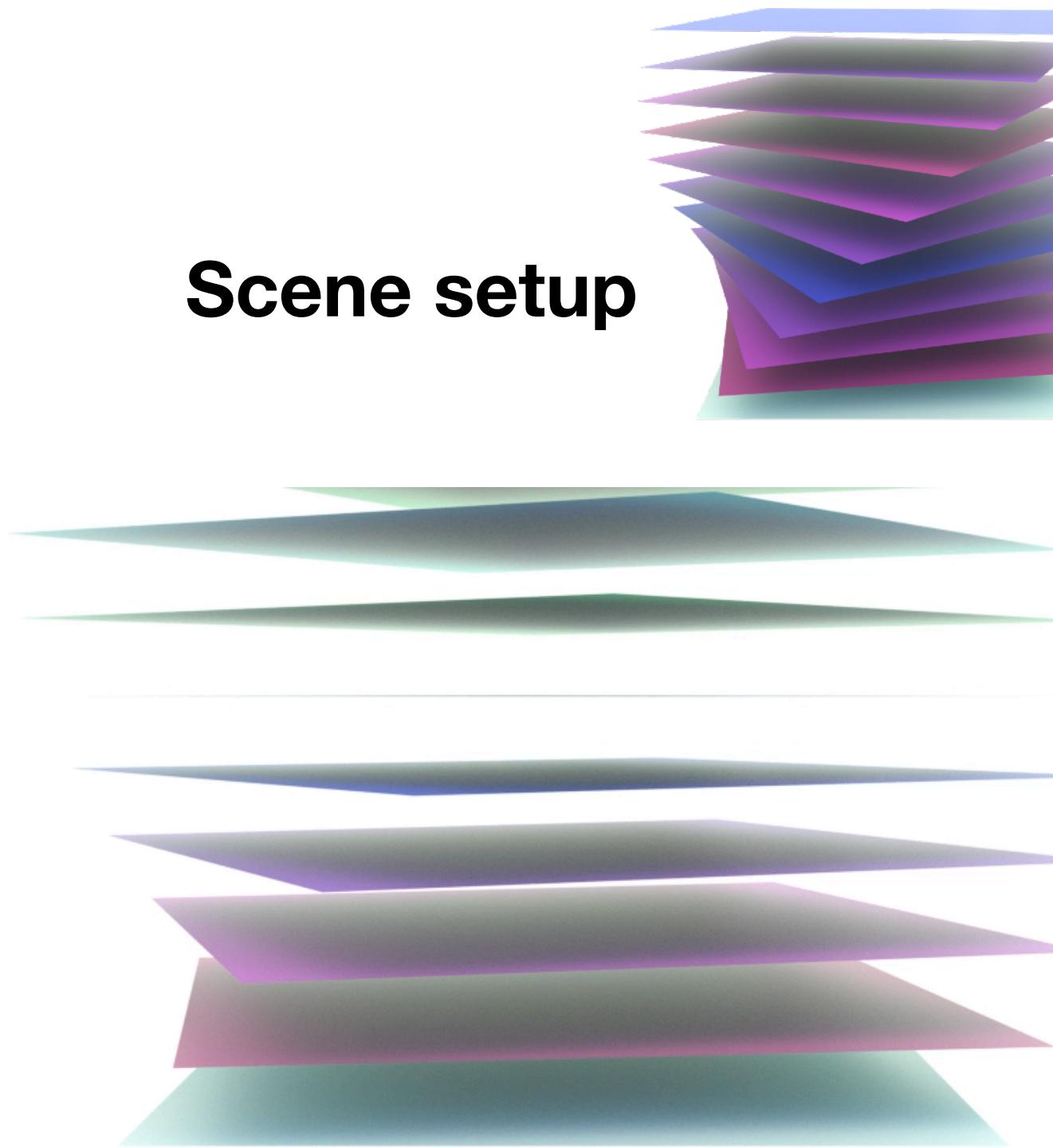
elastic thickness

inelastic thickness

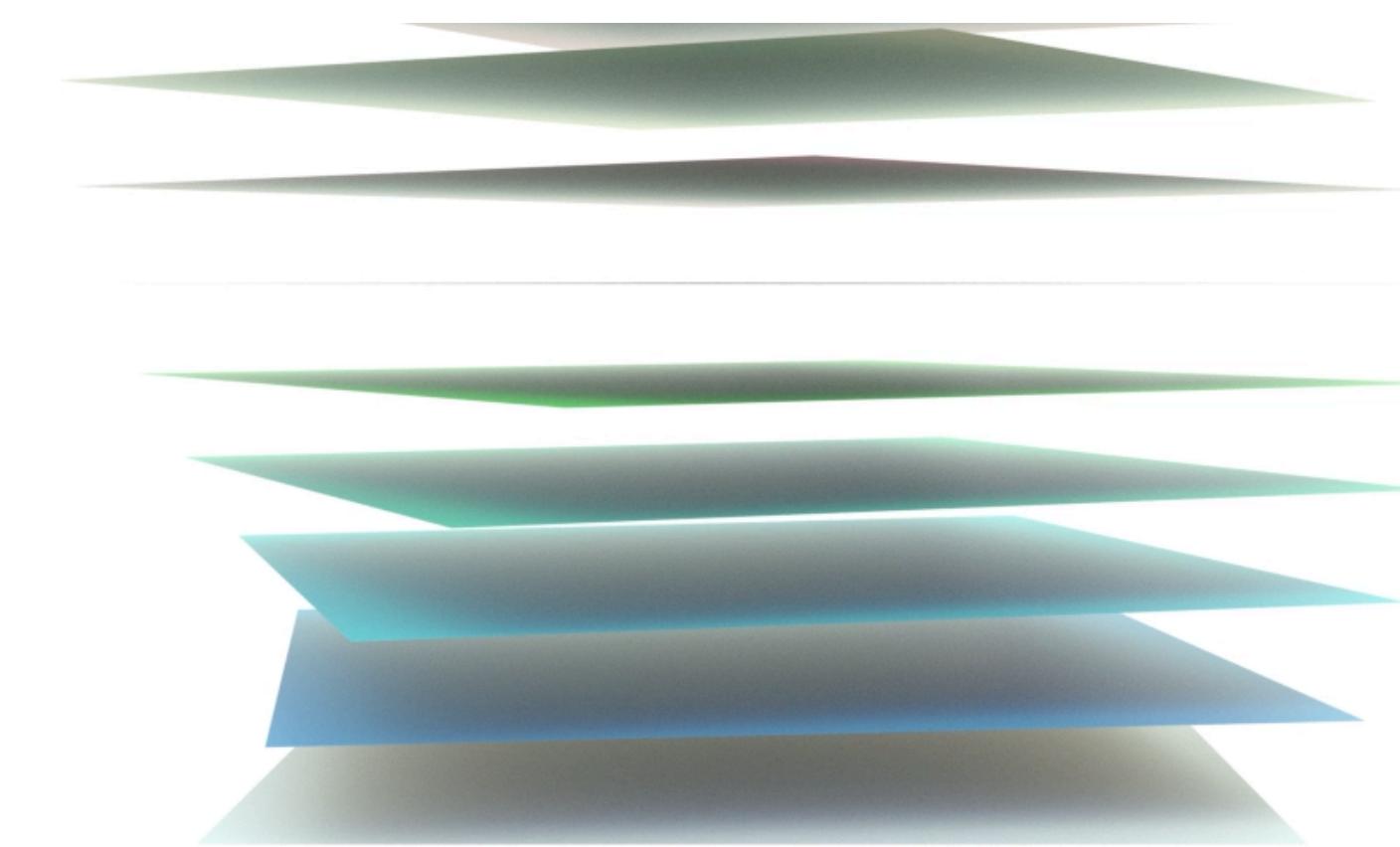
Simulating Cloth using Surface Meshes

Thickness Modeling – Elastic Thickness via Barrier \hat{d}

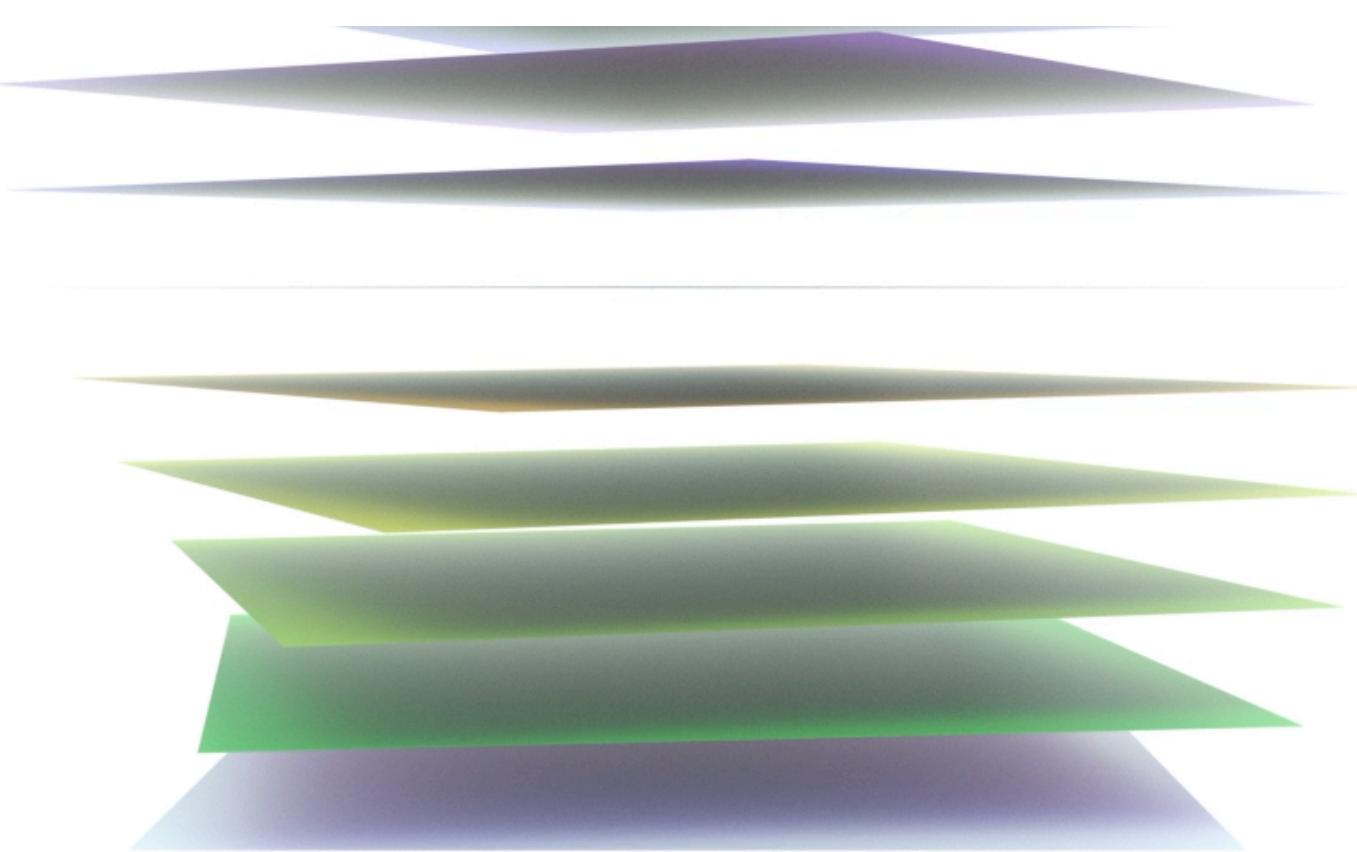
Scene setup



$$\hat{d} = 1\text{mm}, h = 0.04s$$

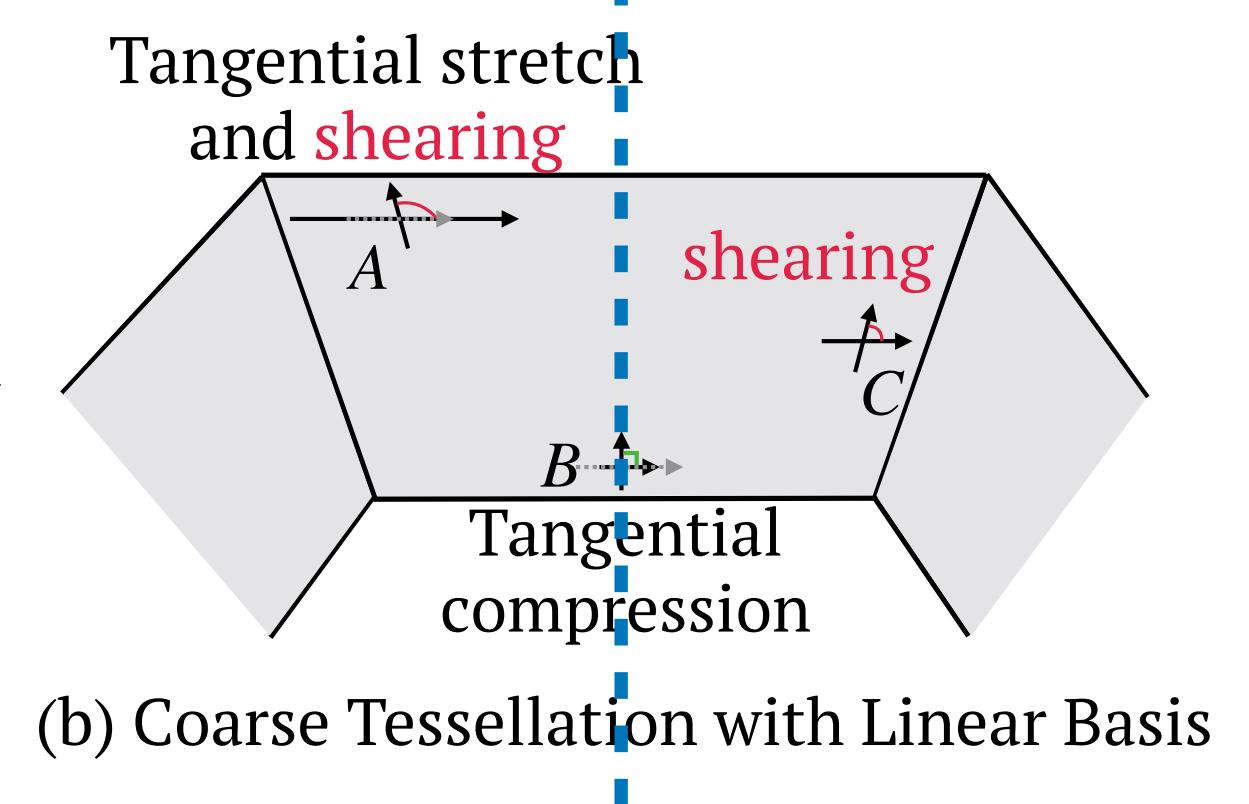
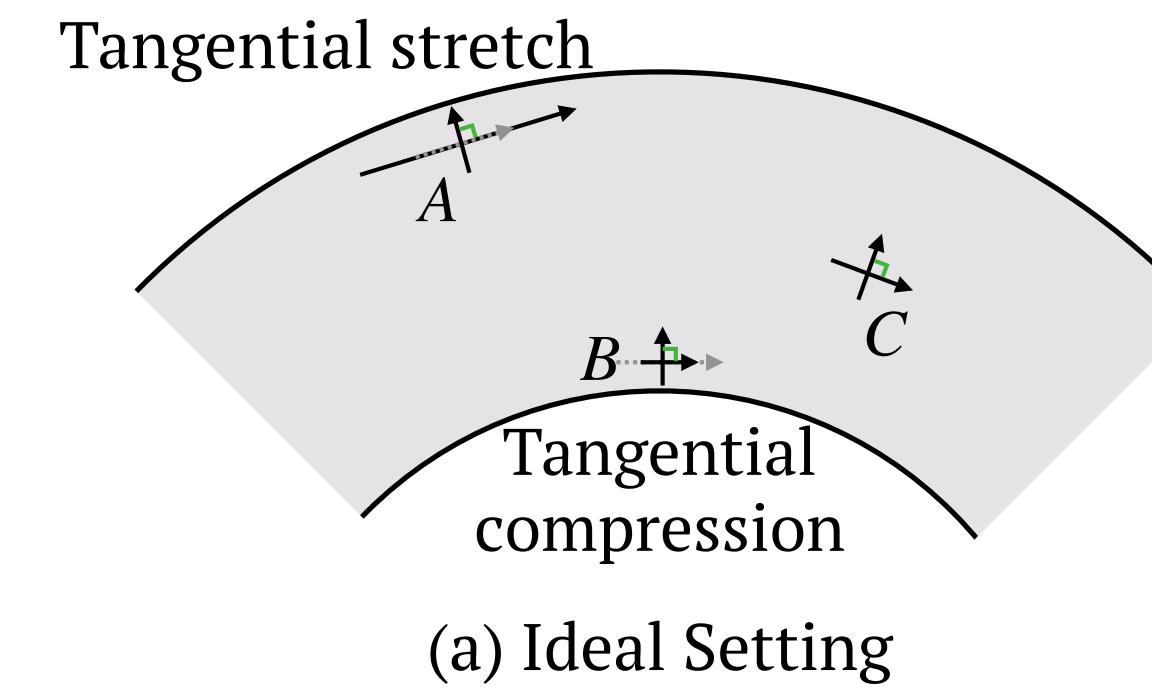
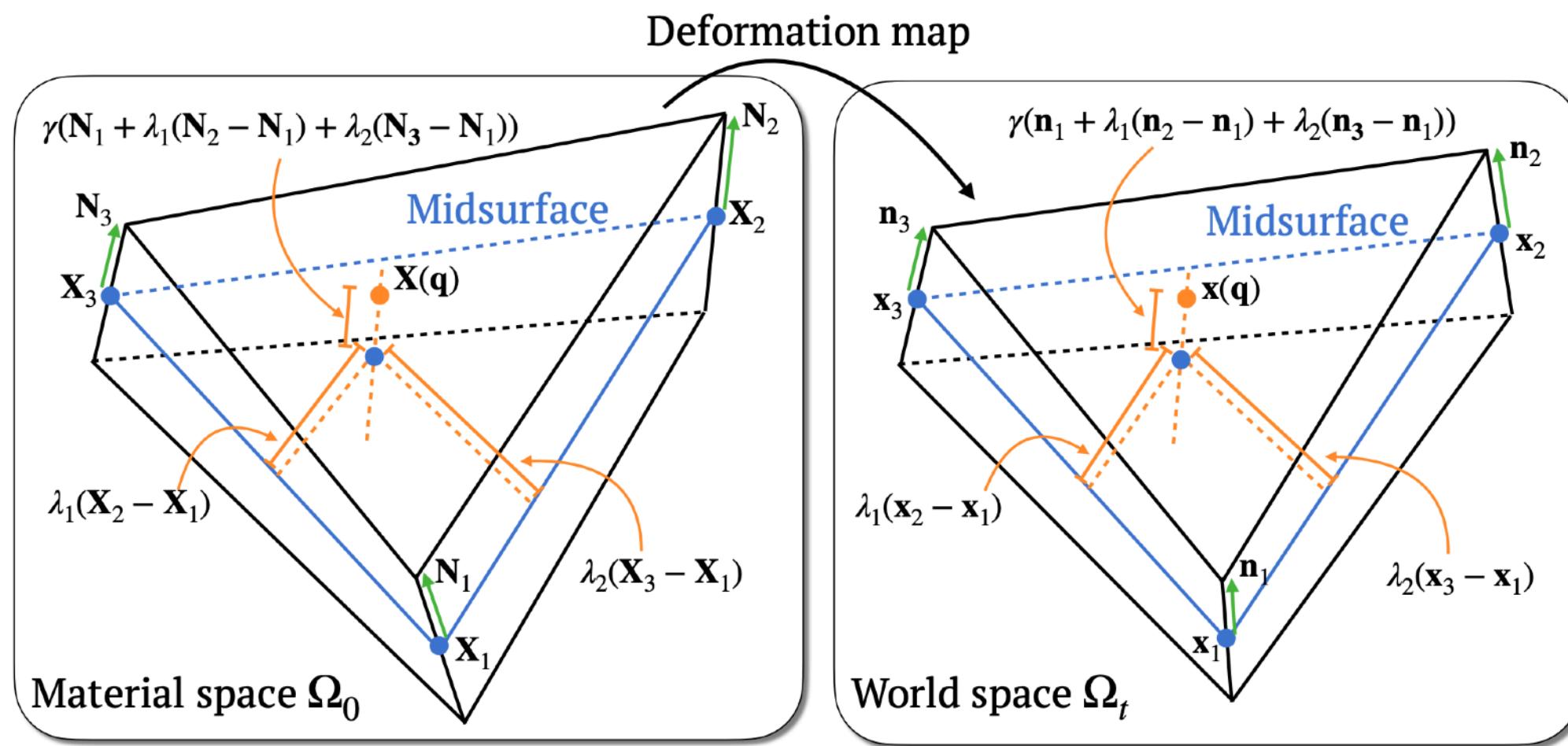


$$\hat{d} = 5\text{mm}, h = 0.04s$$



$$\hat{d} = 10\text{mm}, h = 0.04s$$

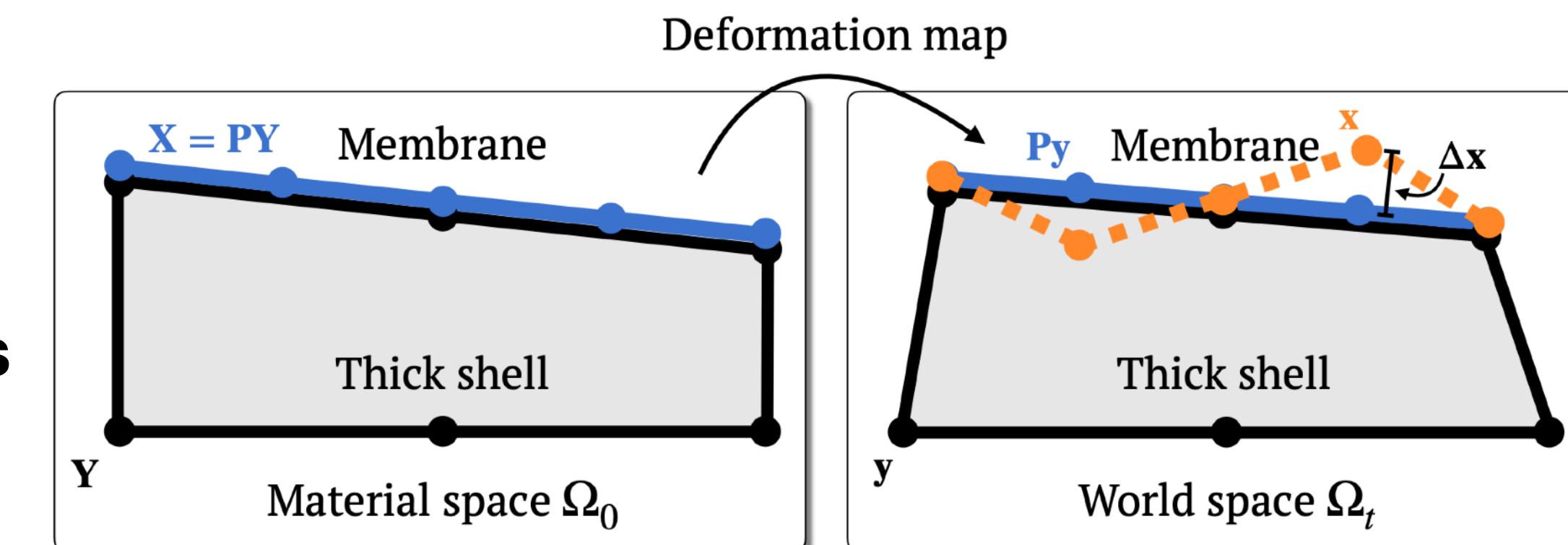
*Simulating Thick Shells [Chen et al. 2023]



Use prism elements to explicitly track thickness

Place quadratures only on the center line to avoid shear locking

Couple with a fine thin shell to simulate wrinkles

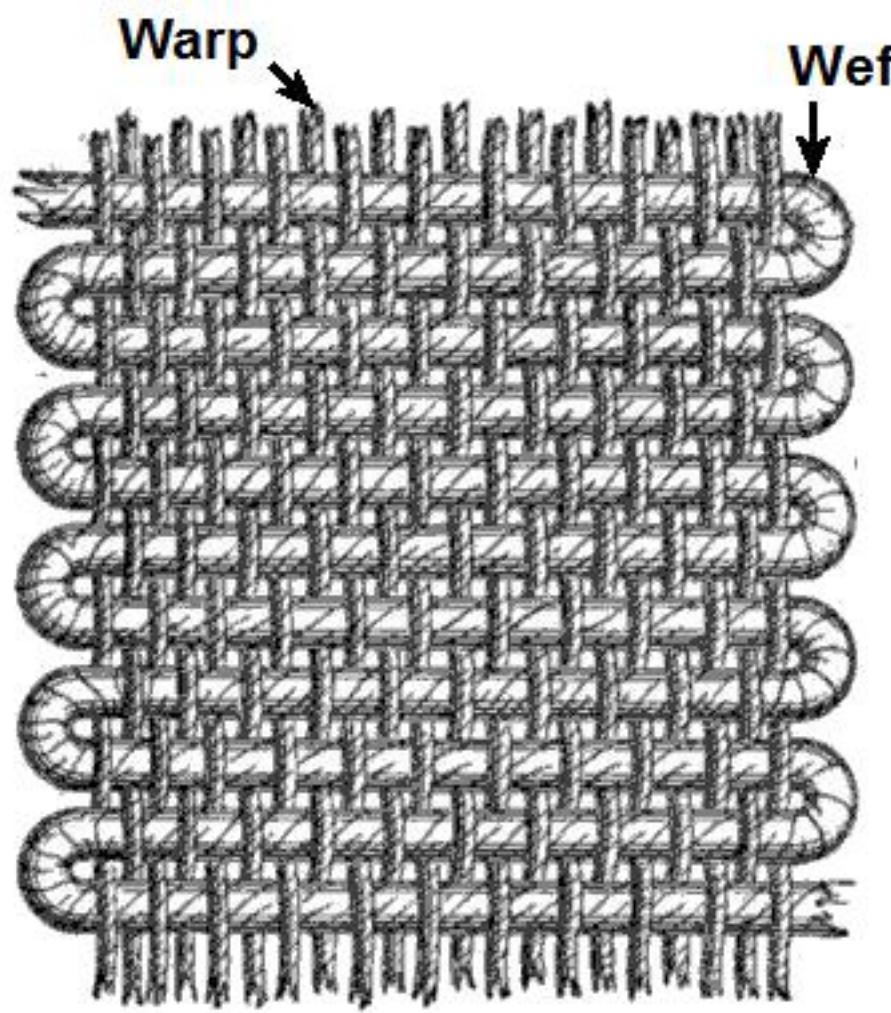


*Simulating Thick Shells [Chen et al. 2023]



Simulating Yarn-Level Cloth

Because of the knitting pattern, cloth is anisotropic

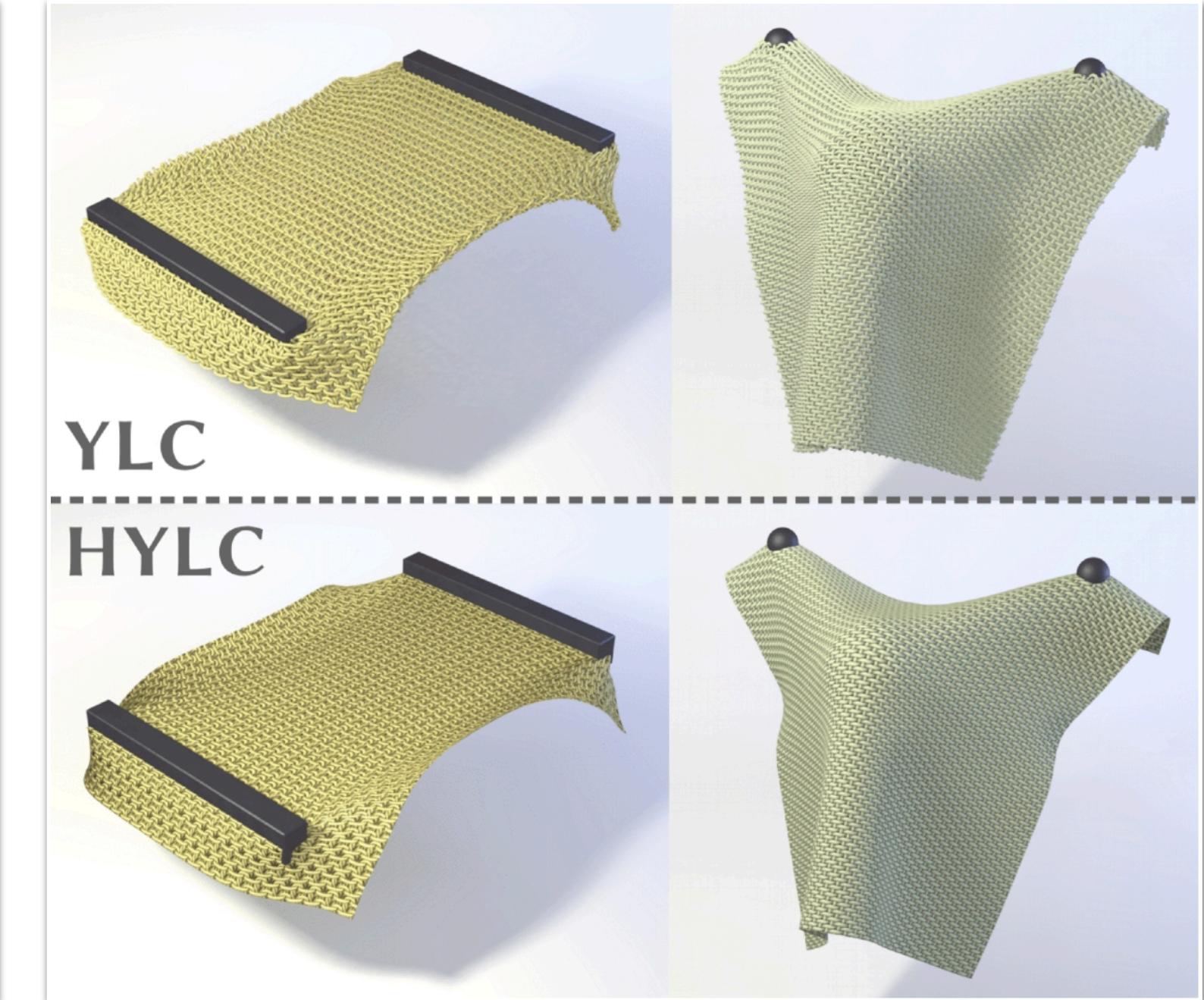


Can directly simulate these yarns!



Figure 9: Scarf: Our contact model scales to support the complex contact and folding that occurs in cloth.

[Kaldor et al. 2008]



[Sperl et al. 2020]

Kaldor, Jonathan M., Doug L. James, and Steve Marschner. "Simulating knitted cloth at the yarn level." ACM SIGGRAPH 2008 papers. 2008. 1-9.

Sperl, Georg, Rahul Narain, and Chris Wojtan. "Homogenized yarn-level cloth." ACM Trans. Graph. 39.4 (2020): 48.

Topics Today:

- **Thin Shells**
 - ▶ Stretching and Bending
 - ▶ Strain Limiting and Thickness
- **Rods and Particles**

Simulating Slender Rods using Polylines

Discrete Elastic Rods

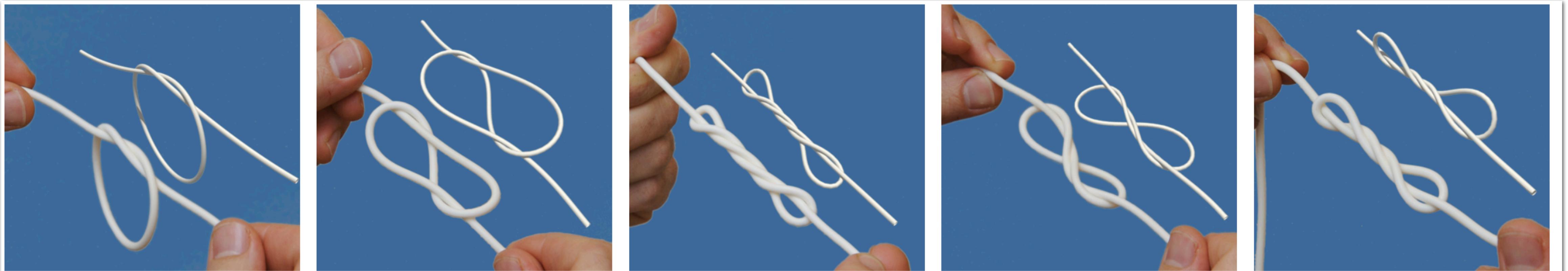


Figure 1: **Experiment and simulation:** A simple (trefoil) knot tied on an elastic rope can be turned into a number of fascinating shapes when twisted. Starting with a twist-free knot (*left*), we observe both continuous and discontinuous changes in the shape, for both directions of twist. Using our model of Discrete Elastic Rods, we are able to reproduce experiments with high accuracy.

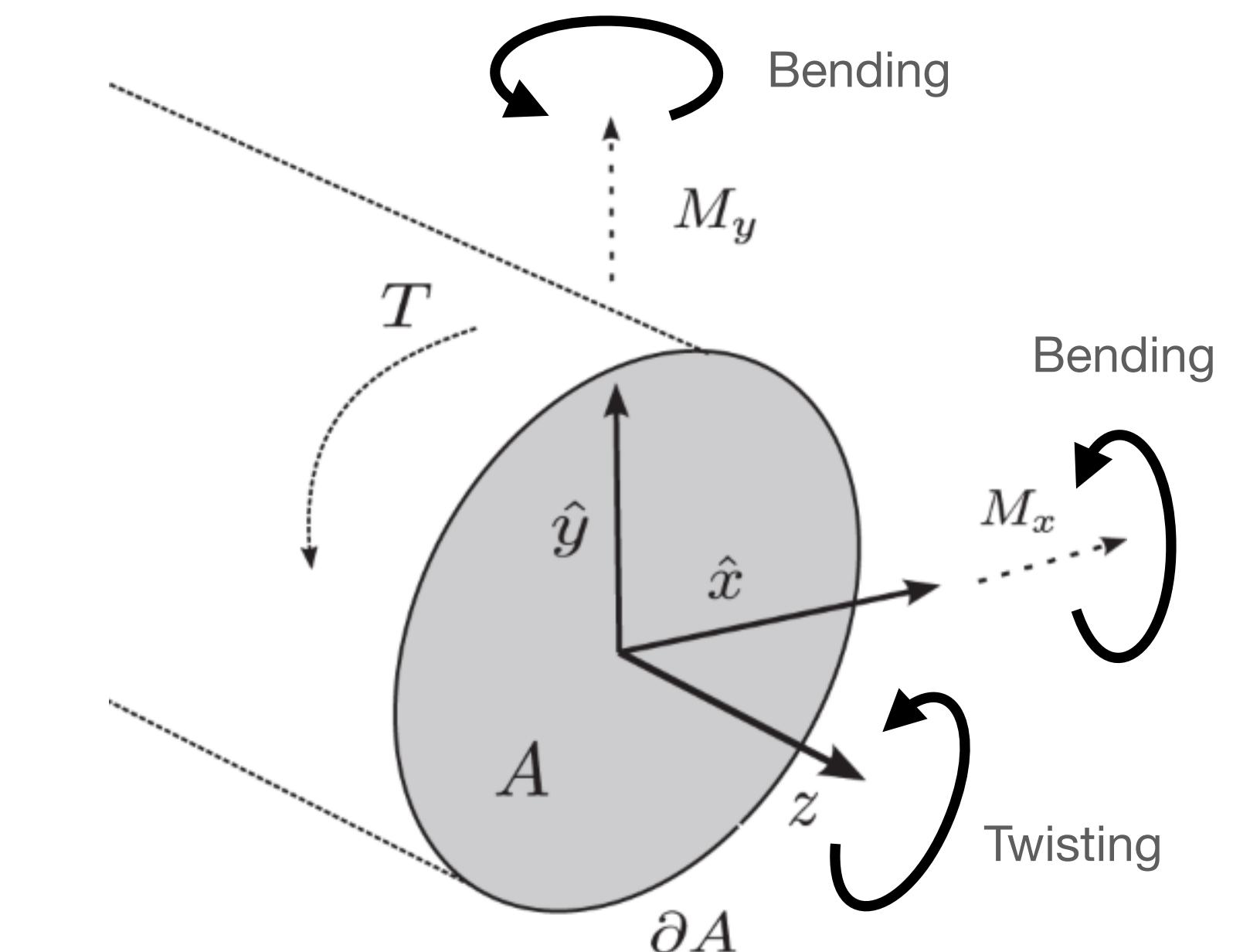
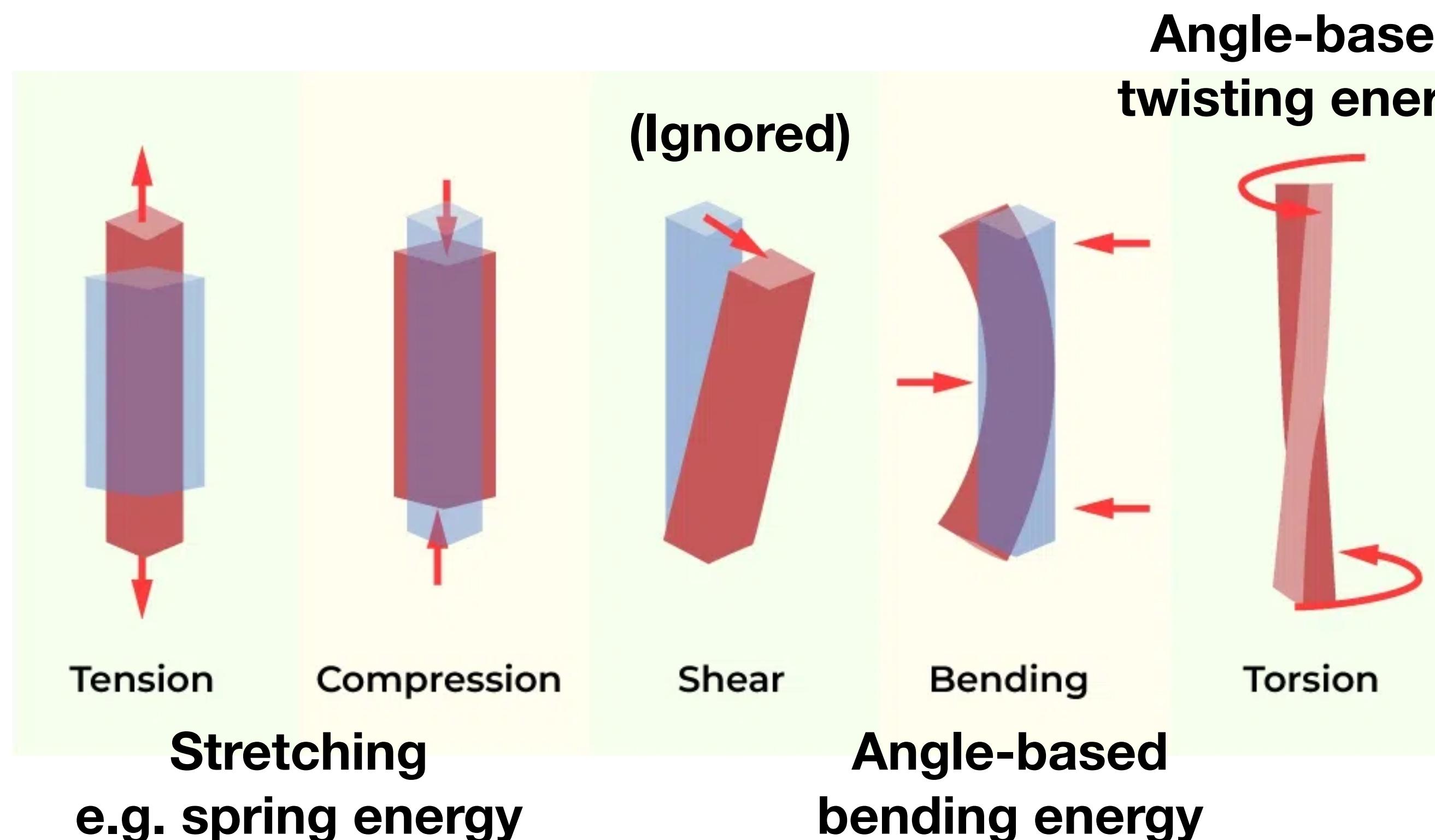
[Bergou et al. 2008]

Strain energy decomposed into **stretching**, **bending**, and **twisting** energies.

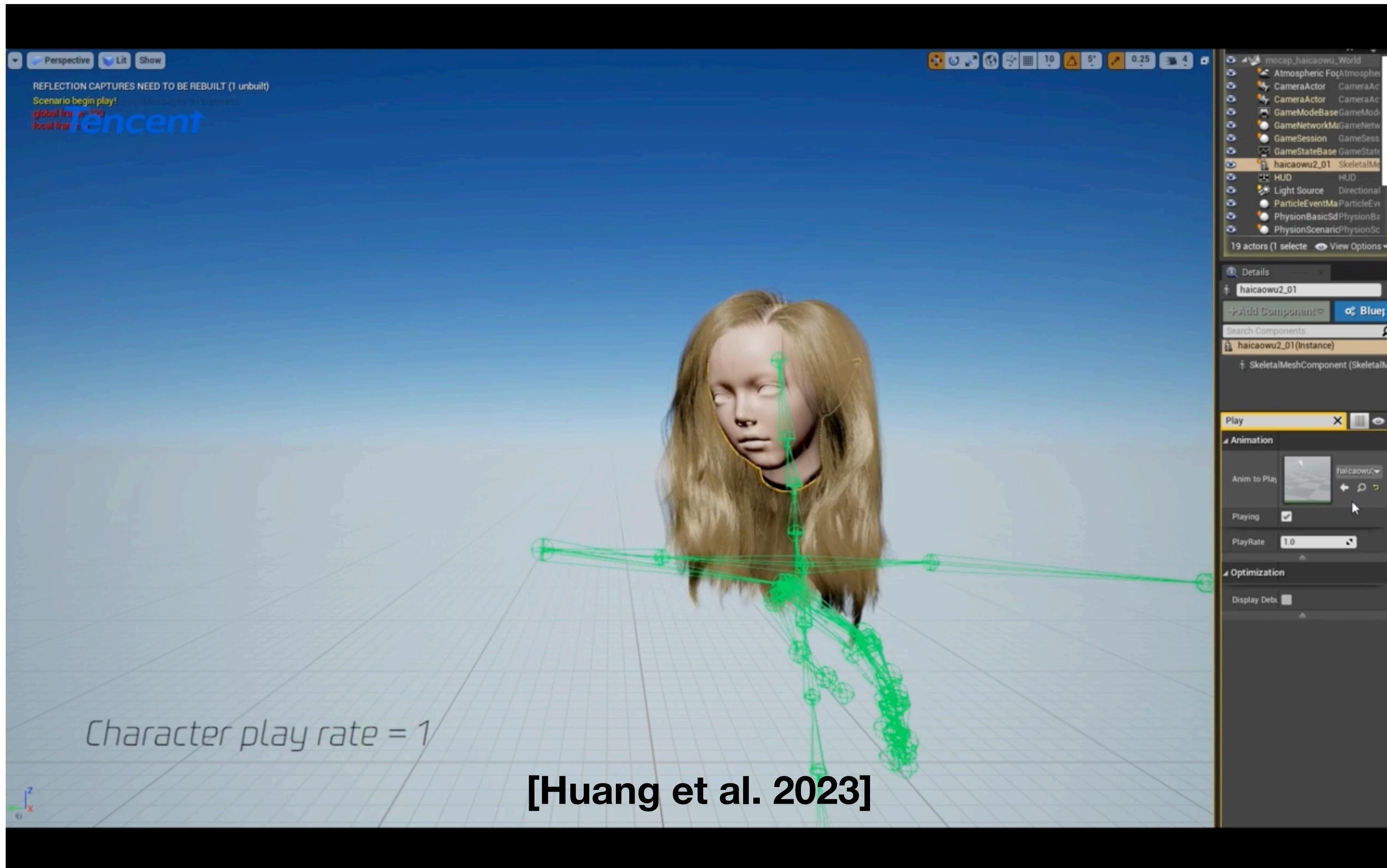
Simulating Slender Rods using Polylines

Discrete Elastic Rods – Stretching, Bending, Twisting

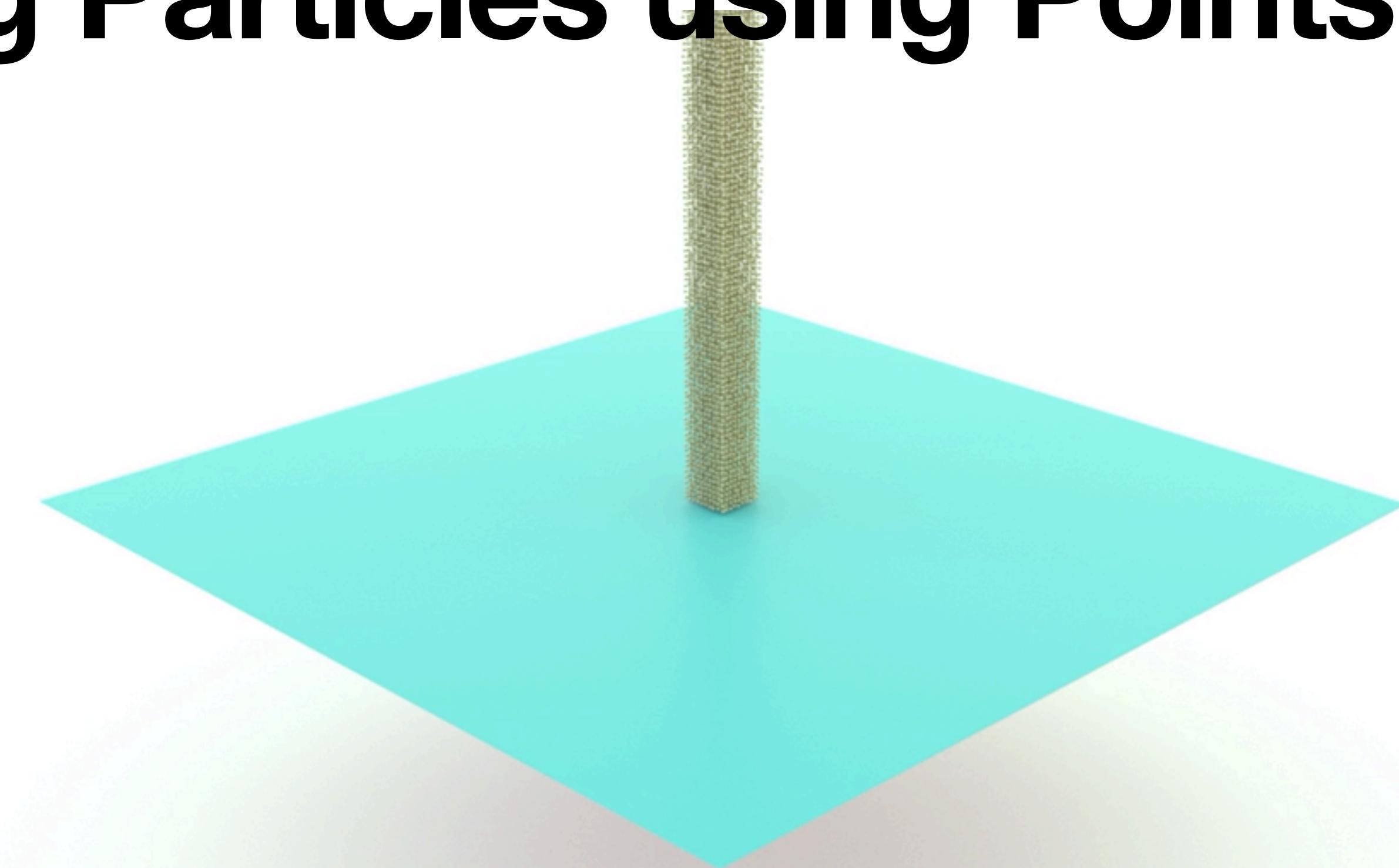
- Idea: use rotation angles of local frames to measure bending and twisting deformation:



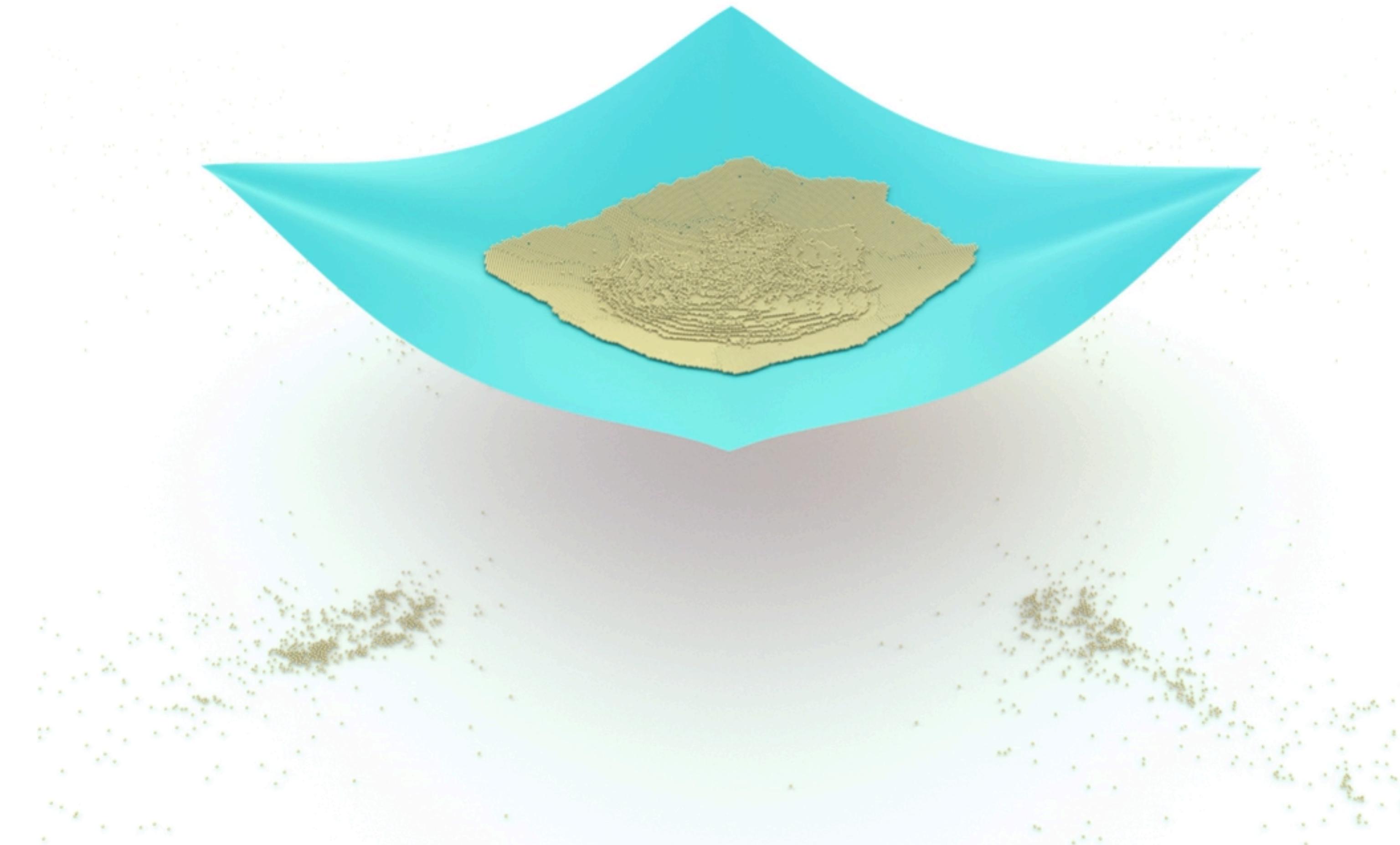
Simulating Hairs using Polylines



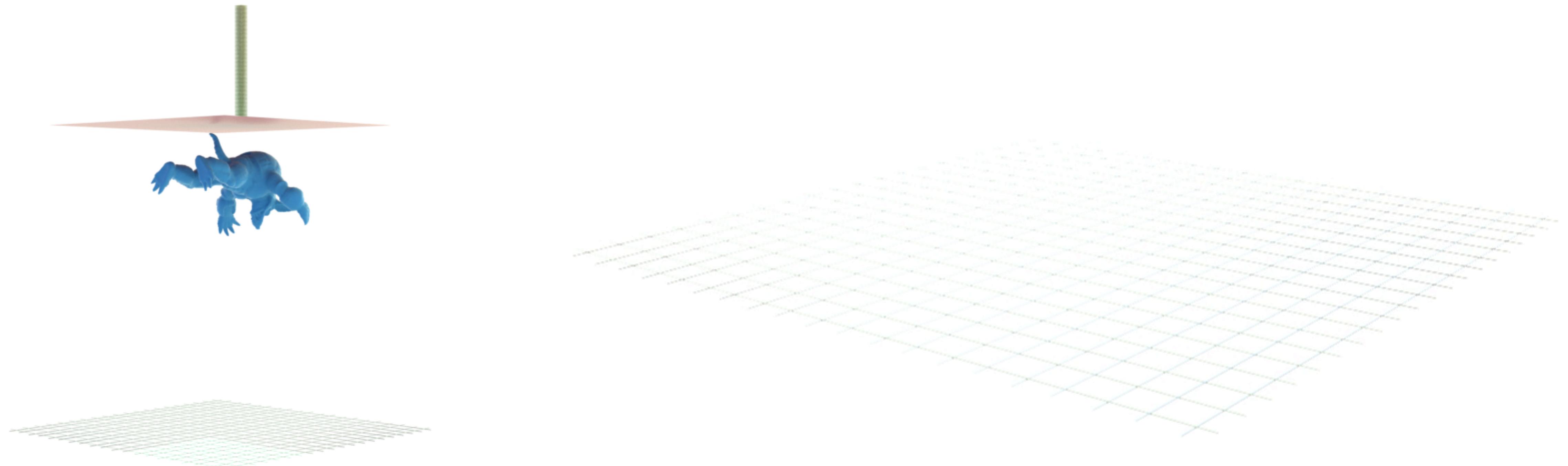
Simulating Particles using Points



Simulating Particles using Points



“All-In” Coupled using IPC



Scene setup

Topics Today:

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Next Lecture: Fluids

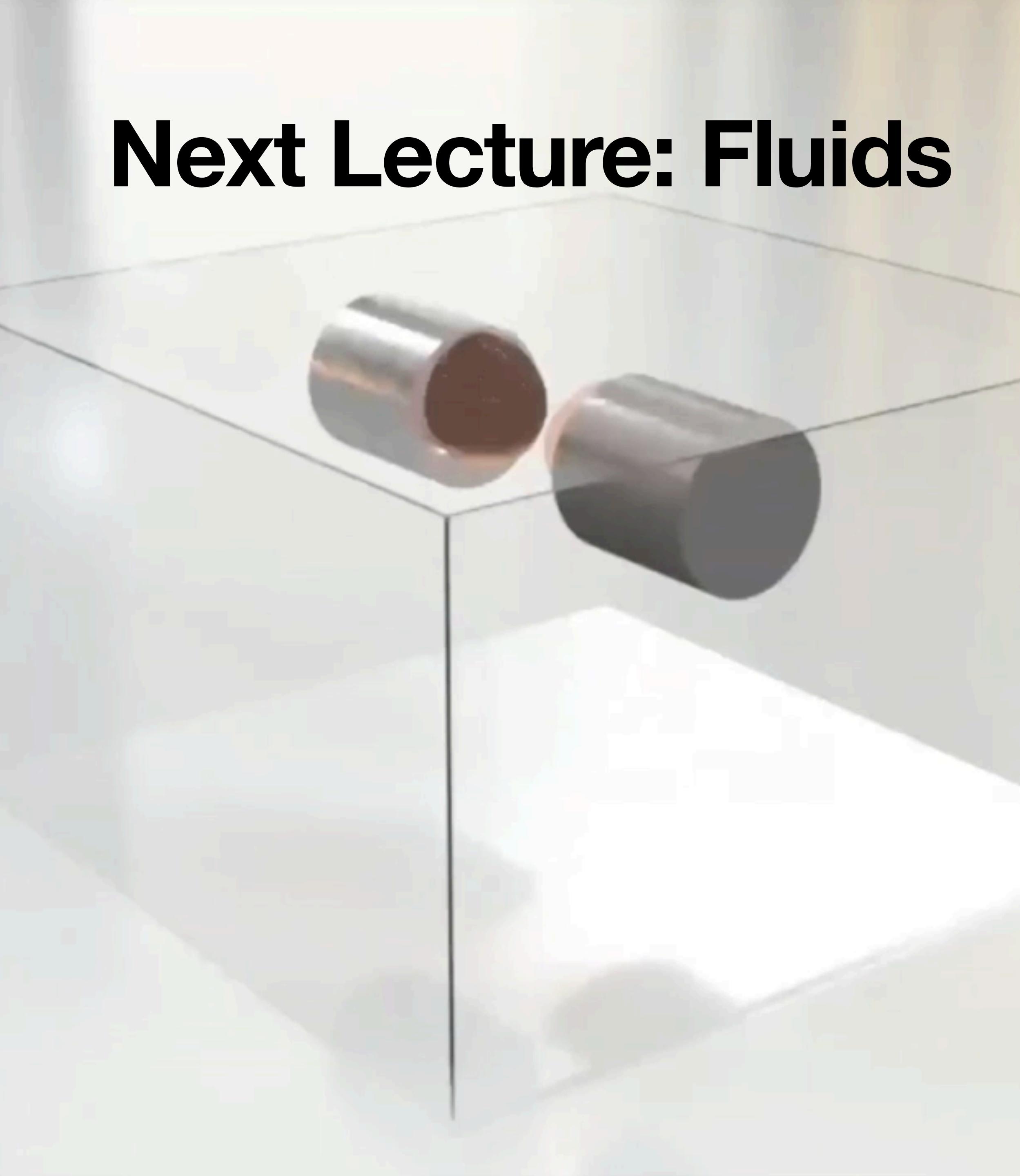


Image Sources

- <http://viterbi-web.usc.edu/~jbarbic/femdefo/barbic-courseNotes-modelReduction.pdf>
- [https://www.researchgate.net/publication/332914440_Port-Hamiltonian formulation and symplectic discretization of plate models Part II Kirchhoff model for thin plates/figures?lo=1&utm source=google&utm medium=organic](https://www.researchgate.net/publication/332914440_Port-Hamiltonian_formulation_and_symplectic_discretization_of_plate_models_Part_II_Kirchhoff_model_for_thin_plates/figures?lo=1&utm_source=google&utm_medium=organic)
- <http://multires.caltech.edu/pubs/ds.pdf>
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- <https://visualcomputing.ist.ac.at/publications/2020/HYLC/>
- <https://www.cs.columbia.edu/cg/pdfs/143-rods.pdf>
- <https://www.geeksforgeeks.org/stress-and-strain/>
- <https://www.nature.com/articles/s41598-019-52878-z>
- <https://www.youtube.com/watch?v=UDQaw4Ff3sg>